

Signal Theory and Design for Wireless Transmission of Information and Power

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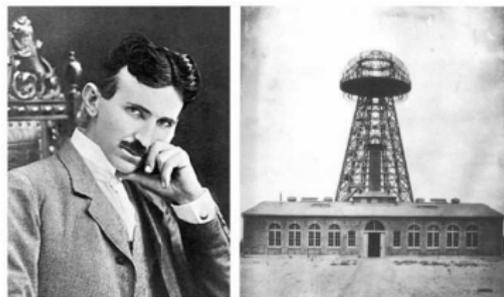
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Wireless is More than just Communications

Radio waves carry both energy and information

Wireless Power Transmission
(WPT)



Tesla 1901

0G

Wireless Information Transmission
(WIT)



Marconi 1896

5G

**Unified Wireless Information and Power Transmission
(WIPT)**

A Missing Signal Theory of Wireless Transmission

Wireless Power Transmission

RF Theory



Signal Theory



Wireless Information Transmission

RF Theory



Signal Theory
(Shannon, ...)



Wireless Information and Power Transmission

Unified Signal Theory



① Signal Design for Wireless Power Transmission

② Signal Design for Wireless Information and Power Transmission

A generic architecture

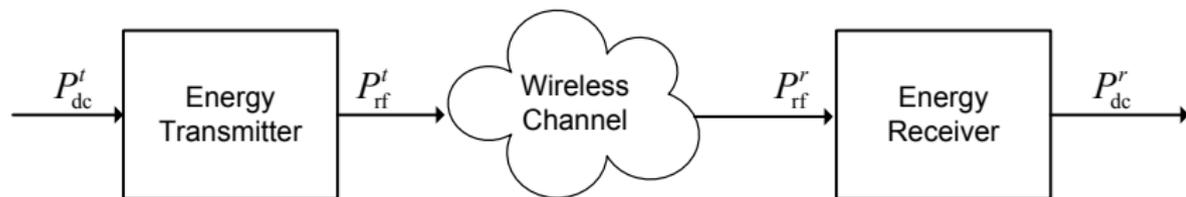


End-to-End Power Transfer Efficiency

$$e = \frac{P_{dc}^r}{P_{dc}^t} = \underbrace{\frac{P_{rf}^t}{P_{dc}^t}}_{e_1} \underbrace{\frac{P_{rf}^r}{P_{rf}^t}}_{e_2} \underbrace{\frac{P_{dc}^r}{P_{rf}^r}}_{e_3}$$

- WEH: no control of e_1 and e_2 .
- WPT: more control of the design and room for enhancement of e

WPT Architecture



Careful! Maximizing e not achieved by maximizing e_1 , e_2 , e_3 independently from each other

- e_1 , e_2 , e_3 coupled due to **nonlinearity**, especially at $1\mu W$ - $1mW$
- e_3 (input signal shape and power) $\rightarrow e_3$ (Tx signal, wireless channel state)
- e_2 (Tx signal, wireless channel state)
- e_1 (Tx signal PAPR)

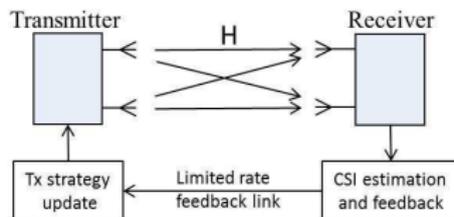
To tackle the listed challenges, we need...

Systematic signal design for WPT to maximize e

Link and system design for WPT: from a rectenna paradigm to a network paradigm

- Multiple transmitters/receivers, coordination among energy transmitters

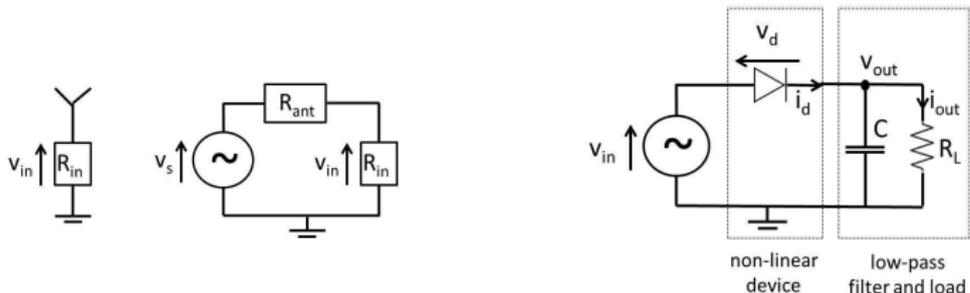
Closed-loop and adaptive WPT



- to support channel feedback/training, energy feedback, charging control
- to flexibly adjust the Tx strategy across space and frequency

Then only, leverage WPT design for SWIPT design (bottom-up approach)

But first, we need a Rectenna Model



Challenge: Relate input signal $y(t)$ to output DC current i_{out}

$$y(t) \rightarrow v_s(t) \rightarrow v_{in}(t) \rightarrow i_d(t) \rightarrow i_{out}$$

Needs to be as tractable and accurate as possible

Output DC Current: time average of the diode current $i_d(t)$

$$i_{out} = \mathcal{E}\{i_d(t)\} \quad \text{proportional to} \quad z_{DC} \approx \sum_{i \text{ even}, i \geq 2}^{n_o} k_i R_{ant}^{i/2} \mathcal{E}\{y(t)^i\}$$

Linear vs Nonlinear Model



Linear Model: Truncate to order 2

$$z_{DC} = k_2 R_{ant} \underbrace{\mathcal{E} \{y(t)^2\}}_{P_{rf}^r}$$

- $\max z_{DC} = \max e_2$ with constant e_3
- Tx strategy that maximizes P_{rf}^r is the same strategy that maximizes P_{dc}^r

Nonlinear Model: Truncate to a higher-order term, e.g. order 4 ($n_o = 4$)

$$z_{DC} = k_2 R_{ant} \underbrace{\mathcal{E} \{y(t)^2\}}_{P_{rf}^r} + k_4 R_{ant}^2 \mathcal{E} \{y(t)^4\}$$

- $\max z_{DC} = \max e_2 e_3 \neq \max e_2$

Waveform Design for WPT

Multi-sine multi-antenna transmit signal (antenna $m = 1, \dots, M$ and sinewave $n = 0, \dots, N - 1$)

$$x_m(t) = \sum_{n=0}^{N-1} s_{n,m} \cos(2\pi f_n t + \phi_{n,m})$$

Received signal after multipath

$$y(t) = \sum_{m=1}^M \sum_{n=0}^{N-1} s_{n,m} A_{n,m} \cos(2\pi f_n t + \underbrace{\phi_{n,m} + \bar{\psi}_{n,m}}_{\psi_{n,m}})$$

Frequency response of the channel of antenna m at ω_n

$$h_{n,m} = A_{n,m} e^{j\bar{\psi}_{n,m}}$$

Goal: design $\{s_{n,m}, \phi_{n,m}\}_{\forall n,m}$ so as to maximize the DC output power subject to average transmit power constraint

Systematic Waveform Design

Design amplitudes and phases to maximize the DC output power subject to Tx power constraint using the linear and nonlinear models

Assume **Channel State Information CSI** (in the form of frequency response $h_{n,m}$) **known to the Tx**

Problem: Maximize the quantity z_{DC}

$$\begin{aligned} \max_{\mathbf{S}, \Phi} \quad z_{DC}(\mathbf{S}, \Phi) &= \underbrace{k_2 R_{ant} \mathcal{E}\{y(t)^2\}}_{\text{Linear term}} + \underbrace{k_4 R_{ant}^2 \mathcal{E}\{y(t)^4\} + \dots}_{\text{Nonlinear terms}} \\ \text{subject to} \quad & \frac{1}{2} \|\mathbf{S}\|_F^2 \leq P \end{aligned}$$

Systematic design? Yes, for any M, N, n_o .

A Toy Example

Assume $N = 2$, $M = 1$ and real frequency domain channel

$$z_{DC}(s_0, s_1) = \underbrace{k_2 R_{ant} / 2 (s_0^2 A_0^2 + s_1^2 A_1^2)}_{\text{Linear term}} + \underbrace{3k_4 R_{ant}^2 / 8 \left[(s_0^2 A_0^2 + s_1^2 A_1^2)^2 + 2s_0^2 s_1^2 A_0^2 A_1^2 \right]}_{\text{Nonlinear term}}$$

Transmit power constraint $s_0^2 + s_1^2 = 2P$

Lagrangian optimization leads to **3 stationary points**:

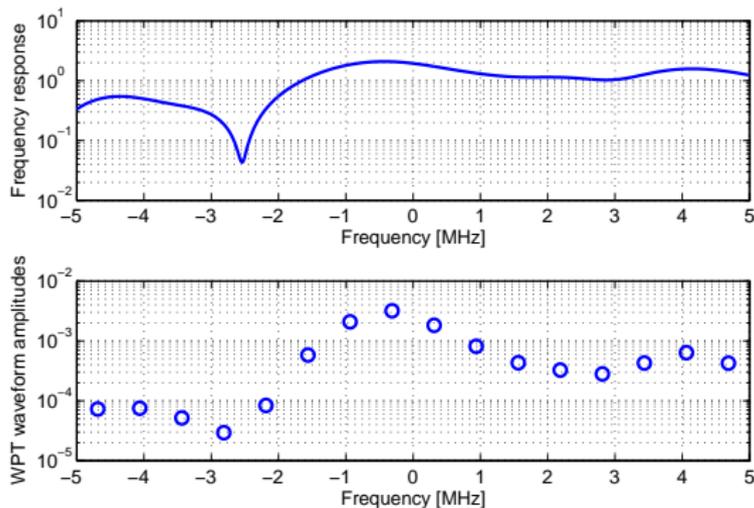
- 1 $(2P, 0)$: Allocate all power to the first sinewave if $A_0 \gg A_1$
- 2 $(0, 2P)$: Allocate all power to the second sinewave if $A_0 \ll A_1$
- 3 (s_0^{*2}, s_1^{*2}) : Allocate power to both sinewaves if $A_0 \approx A_1$

The first two points in general suboptimal with the nonlinear model

Benefits of allocating power over multiple sinewaves for some channel states

Nonlinear model-based design backs up the experimental results

Waveform Illustration



Observation

- 1 Allocate power over multiple sinewaves with more power to frequencies exhibiting larger channel gains
- 2 Optimally exploits **frequency-diversity gain**, spatial **beamforming gain** and **rectifier nonlinearity**

Scaling Laws ($N \gg 1, M = 1, n_o = 4$)

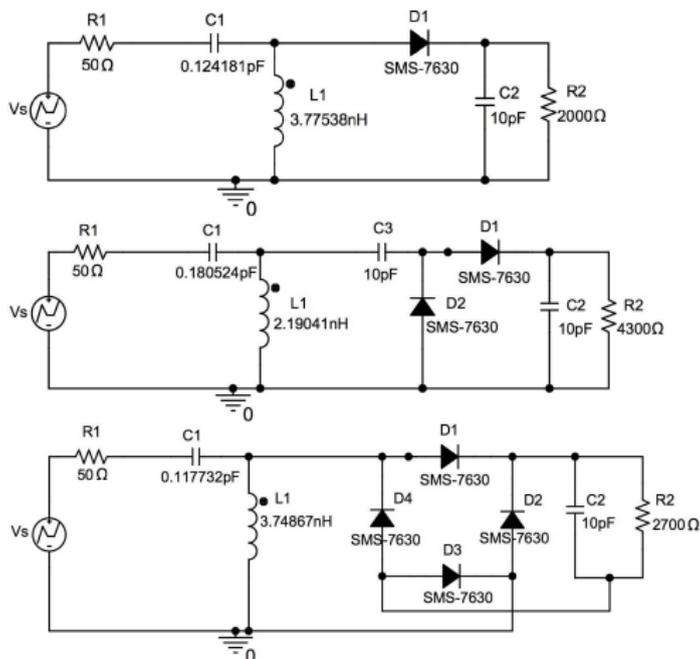
Waveform	Frequency-Flat (FF)	Frequency-Selective (FS)
No CSIT		
z_{DC} NL design	$k_2 R_{ant} P + 2k_4 R_{ant}^2 P^2 N$	$k_2 R_{ant} P + 3k_4 R_{ant}^2 P^2$
CSIT		
z_{DC} L design	$k_2 R_{ant} P + 3k_4 R_{ant}^2 P^2$	$k_2 R_{ant} P \log N + \frac{3}{2} k_4 R_{ant}^2 P^2 \log^2 N$
z_{DC} NL design	$k_2 R_{ant} P + 2k_4 R_{ant}^2 P^2 N$	$k_2 R_{ant} P + k_4 R_{ant}^2 P^2 N$

Observation

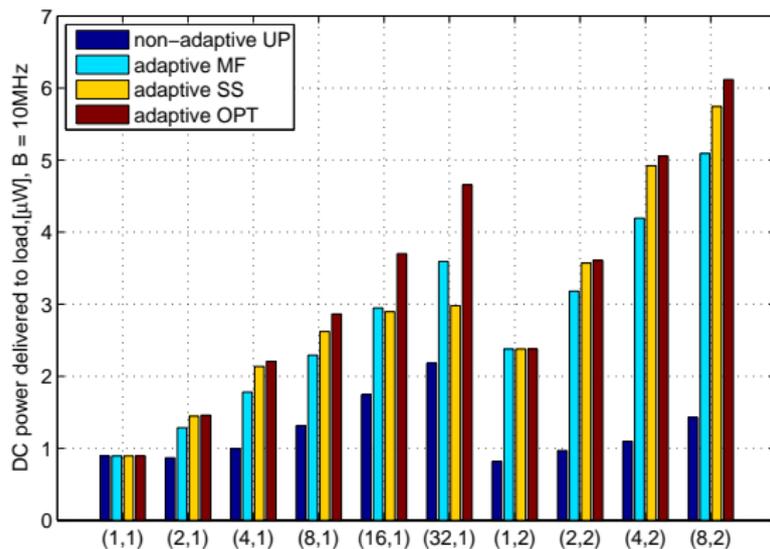
- 1 *Linear increase with N in FF and FS channels.*
- 2 *CSIT not needed in FF channels but needed in FS channels.*
- 3 *linear model-based design leads to significantly lower scaling laws than the non-linear model-based design for FF and FS channels.*
 → *increase in $\log N$ vs N .*

Circuit Evaluations

Single series, voltage doubler and diode bridge rectifiers



Circuit Evaluations



Observation

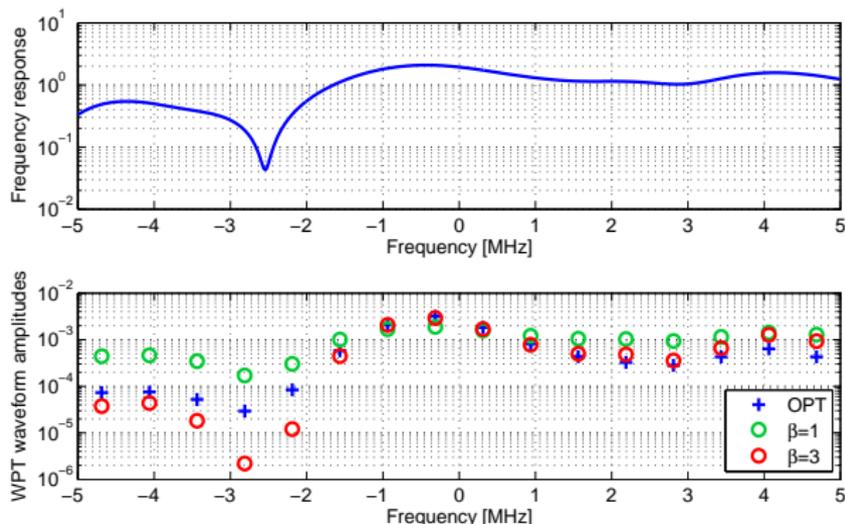
- 1 *Nonlinearity beneficial and exploitable.*
- 2 *Systematic designs exploits BF gain + channel FS + rectifier nonlinearity.*

Low-Complexity Waveform Design

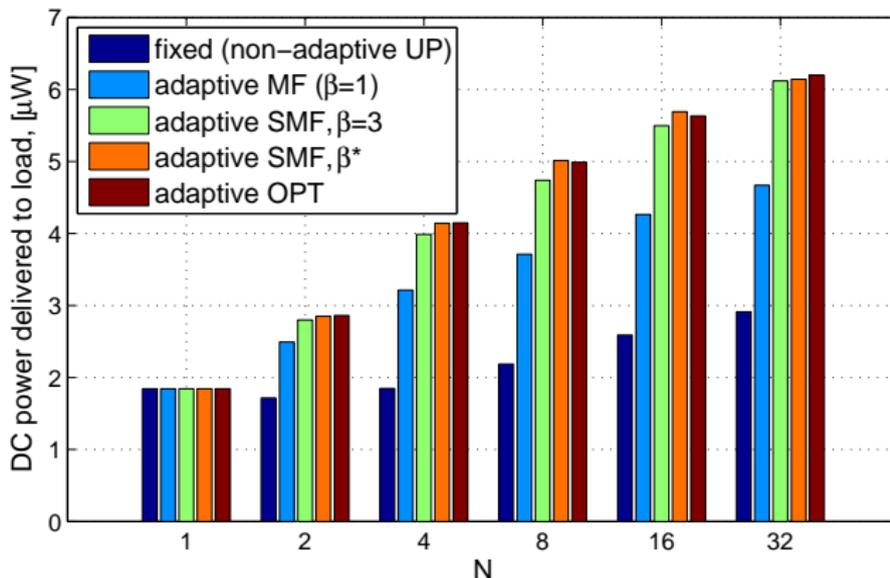
So far, not implementation friendly, difficult to tackle large-scale system

Low-Complexity Adaptive Multisine Waveform

- Idea: allocate more power to frequencies exhibiting larger channel gains
- Scaled Matched Filter (SMF): $s_n = cA_n^\beta$ with c a constant
- A_n^β : amplify strong frequency components and attenuate weak ones



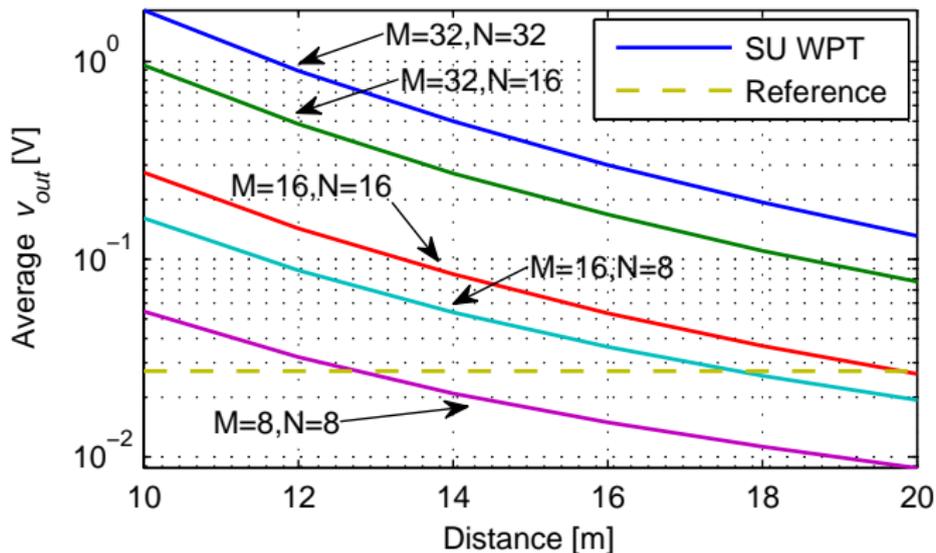
Circuit Evaluations



Observation

- 1 *SMF very close to OPT despite much lower design complexity*
- 2 *Waveform design holds for single and multiple-diode rectennas*

Large-Scale WPT Architecture



Observation

- 1 Significant benefits of the architecture to **boost the end to end power transfer efficiency and the transmission range**

Modulation Design for WPT

Energy modulation in single-carrier/sinewave transmission to **boost** e_3 ?

Induce fluctuations of the transmit signal

Recall $z_{DC} = k_2 R_{ant} \mathcal{E} \{y(t)^2\} + k_4 R_{ant}^2 \mathcal{E} \{y(t)^4\}$

Design modulation/**input distribution** with **large fourth order moment!**

Flash signaling distribution with following probability mass function (with $l \geq 1$)

$$p_r(r) = \begin{cases} 1 - \frac{1}{l^2}, & r = 0, \\ \frac{1}{l^2}, & r = l\sqrt{P}. \end{cases}$$

Low probability of high amplitude signals

- Average power constant $\mathcal{E} \{r^2\} = P$
- ... but $\mathbb{E} [r^4] = l^2 P^2$, i.e. the larger l , the larger the fourth order moment.

Scaling Laws

Modulation	z_{DC}
Continuous wave (CW)	$k_2 R_{ant} P + 3k_4 R_{ant}^2 P^2$
Complex Gaussian (CG)	$k_2 R_{ant} P + 6k_4 R_{ant}^2 P^2$
Real Gaussian (RG)	$k_2 R_{ant} P + 9k_4 R_{ant}^2 P^2$
Flash signaling l	$k_2 R_{ant} P + 3l^2 k_4 R_{ant}^2 P^2$

Observation

- 1 From 2nd order term: Modulated/Unmodulated carriers equally suitable.
- 2 From 4th order term: **Modulated better than Unmodulated.**
- 3 Gain of modulation comes from large fourth order moment.

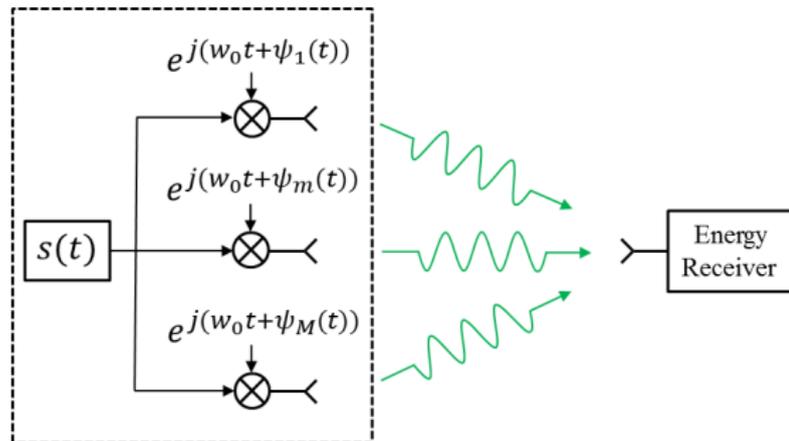
Circuit Evaluations

Transmission type	Delivered DC Power (μW)
Continuous wave (CW)	1.0959
Complex Gaussian (CG)	1.5296
Real Gaussian (RG)	1.7547
Flash signaling $l = 2$	2.6899
Flash signaling $l = 3$	3.4262
Flash signaling $l = 4$	3.4884
Flash signaling $l = 5$	3.2965

Energy modulation gives a 250% gain over CW

Rectenna **nonlinearity favors distributions with a large fourth moment!**

Transmit Diversity for WPT



Energy transmitter with transmit diversity

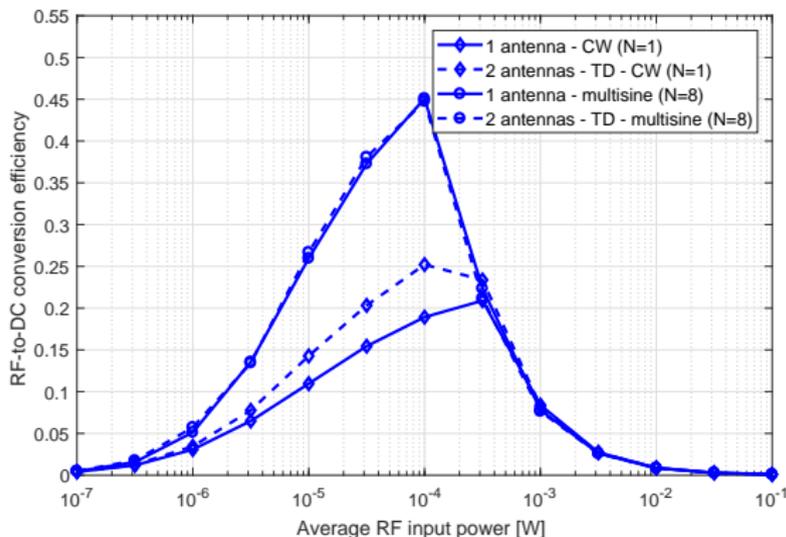
Multiple **dumb** antennas to induce fast fluctuations of the wireless channel

Fluctuations **boost** e_3 thanks to EH nonlinearity

Multiple antenna but **no CSIT** (in contrast to beamforming)

Multiple transmit antennas be useful to WPT in the absence of CSIT!

Increase in RF-to-DC conversion efficiency



35% gain with two antennas over one antenna

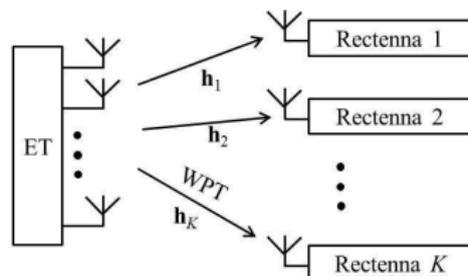
Very low implementation complexity

Well suited for massive IoT for which CSIT acquisition is unpractical

Multi-User WPT Signal Design

Multi-User WPT: WPT to K single-antenna users/rectennas

- Rectennas belong to a single user (i.e. point-to-point MIMO WPT)
- Rectennas spread across multiple users



Trade-off: $z_{DC,q}$ in general depends on $z_{DC,p}$, $p \neq q$

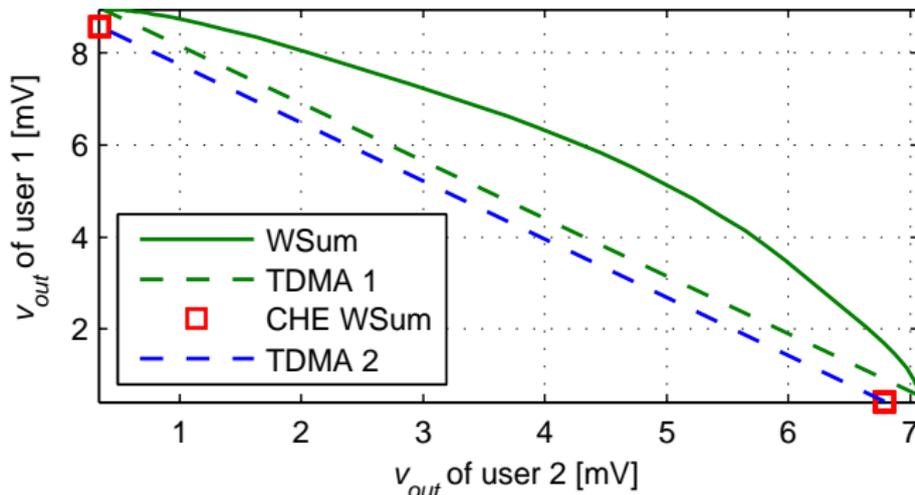
Energy Region \mathcal{Z}_{DC} : set of all rectenna harvested energy ($z_{DC,1}, \dots, z_{DC,K}$) that are simultaneously achievable

Boundary of \mathcal{Z}_{DC} : weighted sum of $z_{DC,k}$ with weights v_k , $k = 1, \dots, K$

$$\max_{\mathbf{S}, \Phi} Z_{DC}(\mathbf{S}, \Phi) = \sum_{k=1}^K v_k z_{DC,k}(\mathbf{S}, \Phi) \quad \text{s.t.} \quad \frac{1}{2} \|\mathbf{S}\|_F^2 \leq P$$

Energy region

Energy region: Achievable v_{out} region, with $M = 20$ and $N = 10$



Observation

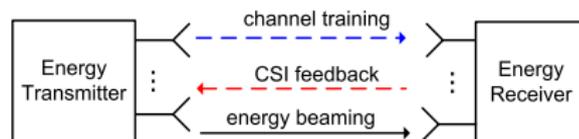
- 1 Achievable energy region with WSum larger than that of TDMA

Channel Acquisition for WPT

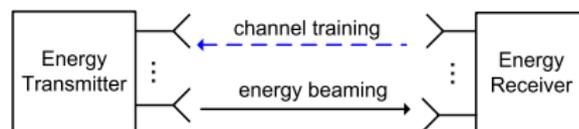
Waveform/beamforming requires **Channel State Information (CSI)** at Tx

Unique considerations

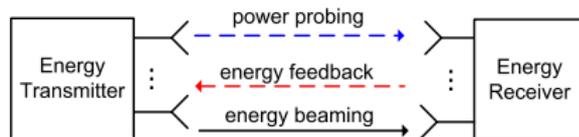
- **CSI at (energy) receiver:** not required for WPT
- **Net energy maximization:** to balance the energy overhead for CSI acquisition and the energy harvested with CSI-based signal design
- **Hardware constraint:** no/low signal processing capability for low-cost ERs



(a) Forward-link training with CSI feedback



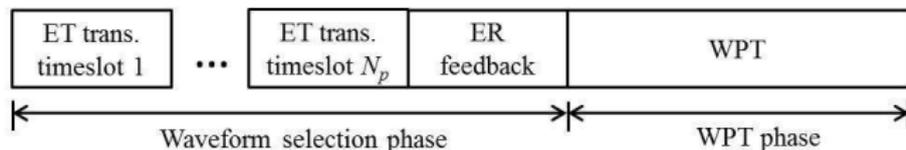
(b) Reverse-link training with channel reciprocity



(c) Power probing with energy feedback

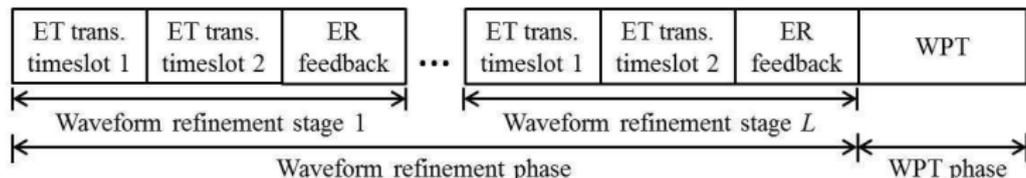
Waveform for WPT with Limited Feedback

Waveform Selection-based WPT



- Waveform precoders: a predesigned N_p -codeword codebook

Waveform Refinement-based WPT



- Waveform precoders: a predesigned tree-structured codebook

Waveform codebook design reminiscent of Lloyd Algorithm.

Challenge: finding the centroid subject to nonlinearity.

Prototyping and Experimentation of Closed-Loop WPT

Demonstrate the first prototype of a closed-loop WPT system with adaptive waveform optimization based on CSI acquisition

Establish an **experimental environment for closed-loop WPT** with waveform optimization

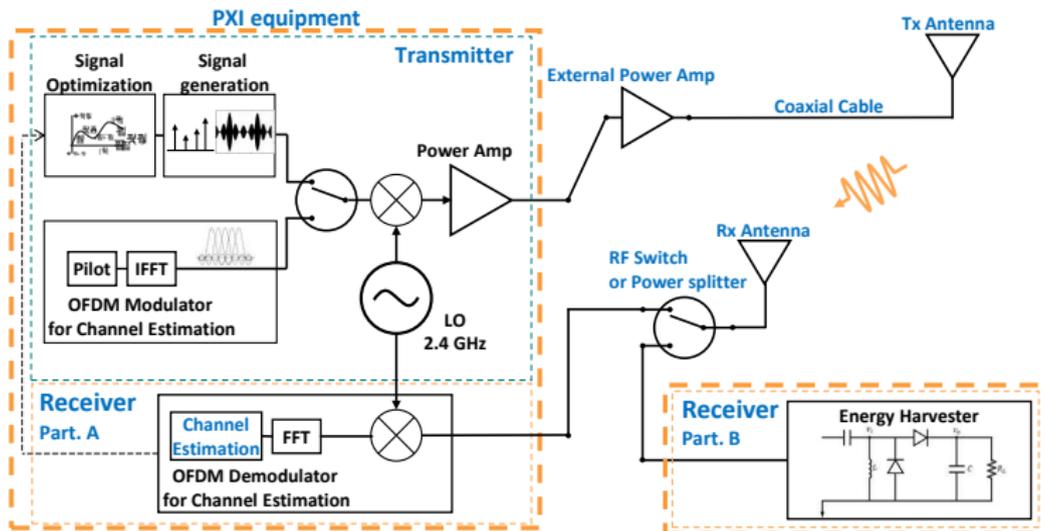
- Design optimized multi-sine RF Tx
- Implement CSI acquisition/channel estimator
- Design efficient rectenna

Verify advantages of systematic signal designs for WPT

- waveform, beamforming, modulation, transmit diversity

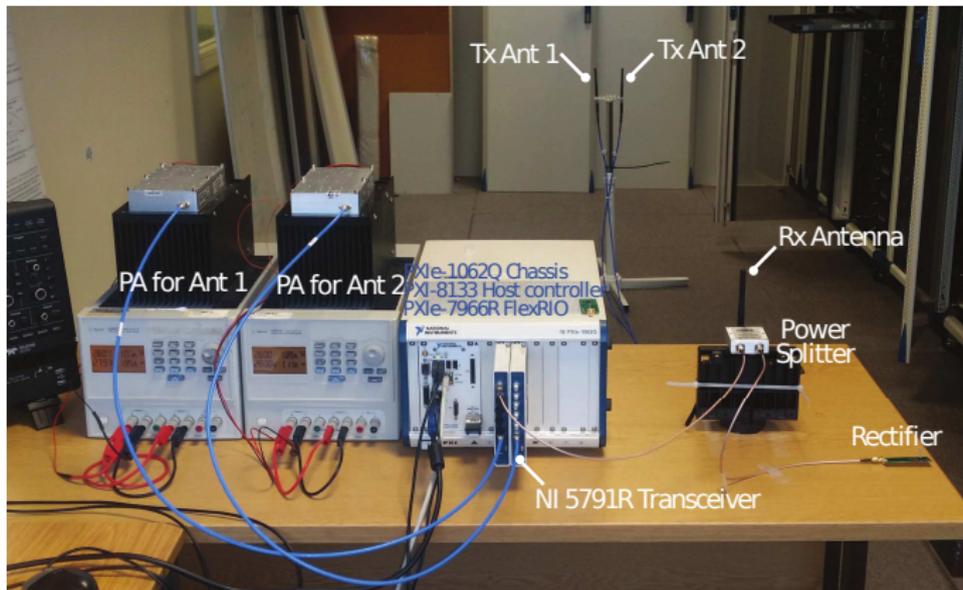
Measurements confirm theory: gains very promising

Prototype Architecture

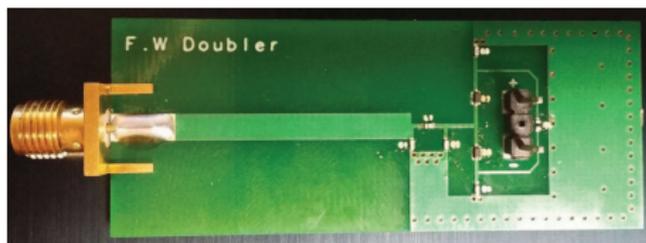
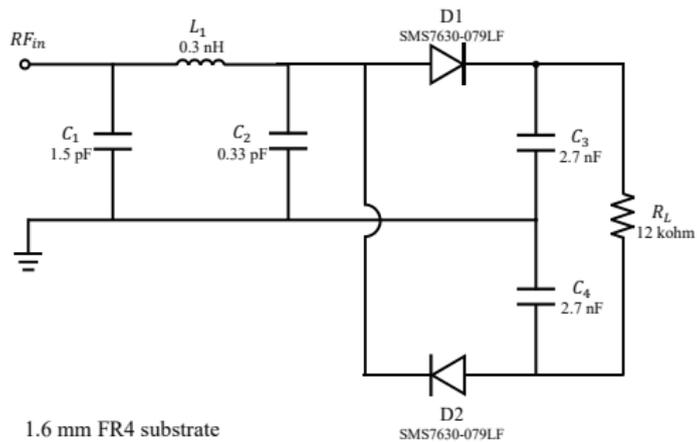


- The system operates in 2.4 GHz ISM band
- Software Defined Radio (SDR) used for transmitter and channel estimator. NI FlexRIO (PXI-7966R) and transceiver module (NI 5791R)
- Channel estimation and waveform design implemented in LabVIEW

Actual Prototype

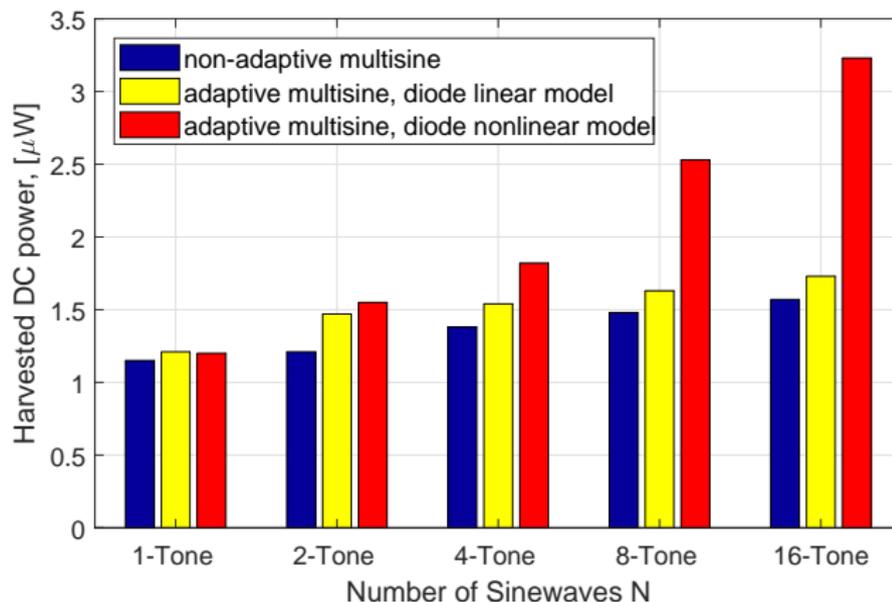


Rectifier



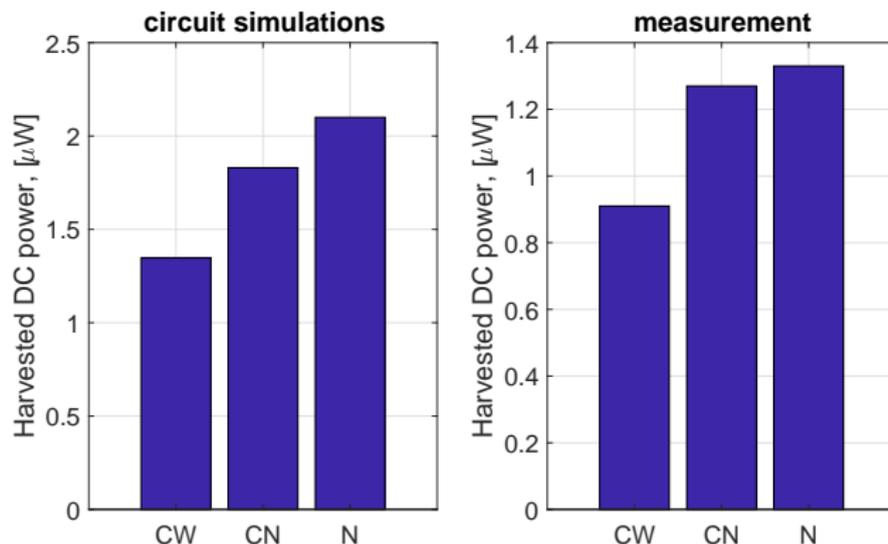
Measurement Results: Waveform

Received DC power as a function of N with 10 MHz bandwidth in NLoS



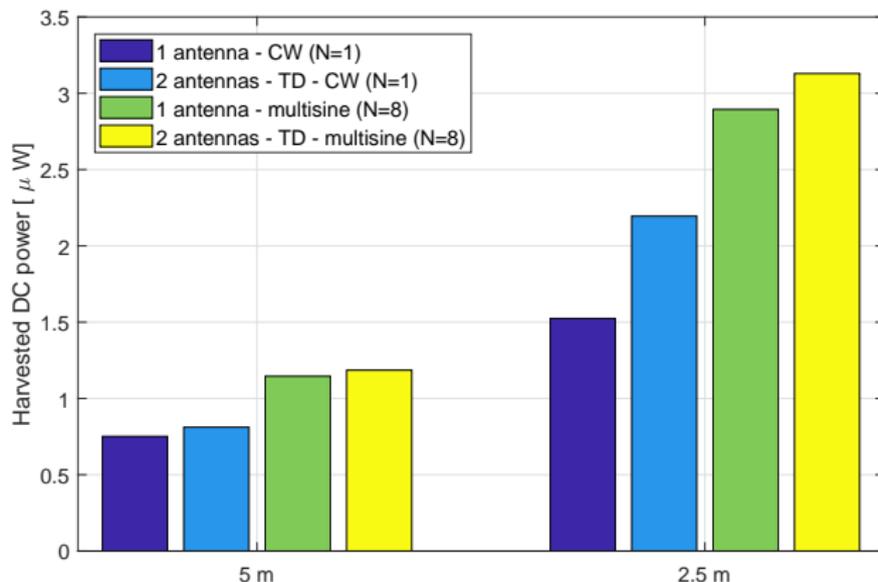
Measurement Results: Modulation

Received DC power as a function of modulation (CW refers to continuous wave, CN to CSCG input, and N to real Gaussian input).

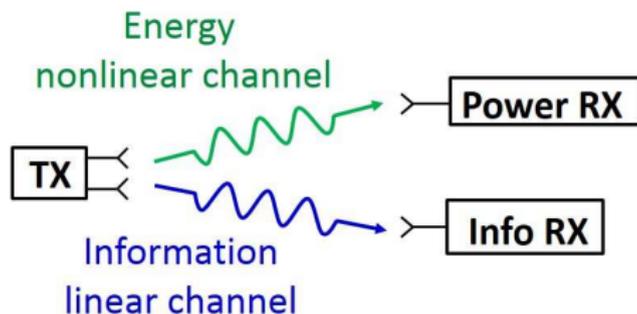


Measurement Results: Transmit Diversity

Received DC power with a continuous wave (CW), transmit diversity ($M = 2$) with continuous wave, multisine ($N = 8$) and transmit diversity with multisine ($N = 8$)



Wireless Information and Power Transmission

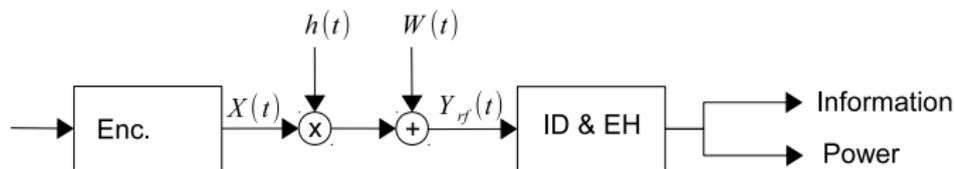


Fundamental tradeoff between rate and harvested DC power?

Unified signal theory and design for WIPT?

Characterizing Fundamental Limits of SWIPT

... in single-carrier frequency-flat AWGN channel with **Nonlinear** EH



Rate-Energy Region: Maximize **information rate** and **delivered power**

- Information rate (R): (Mutual information)

$$R = I(X; Y)$$

- Delivered power (P_{del}): (**Nonlinear** approximation)

$$P_{\text{del}}(X) = \mathcal{E}[k_2 Y_{\text{rf}}(t)^2 + k_4 Y_{\text{rf}}(t)^4]$$

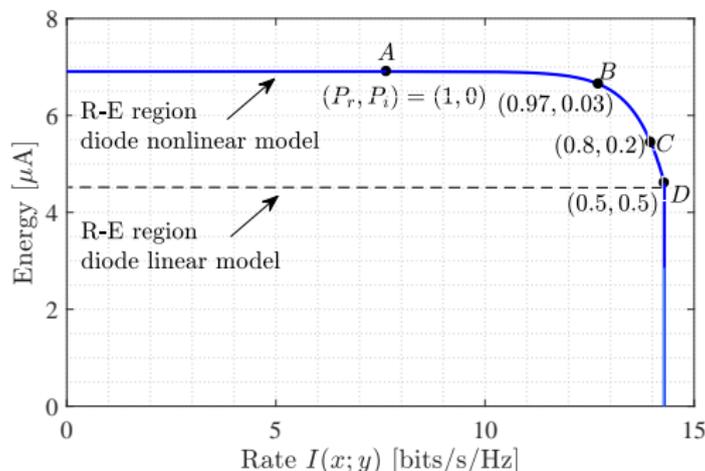
- Problem

$$\sup_{p_X(x)} I(X; Y)$$

$$\text{s.t.} \quad \begin{cases} E[|X|^2] \leq P_{\text{rf}}^t \\ P_{\text{del}}(X) \geq P_d \end{cases}$$

Characterizing Fundamental Limits of SWIPT

Gaussian inputs: $\Re\{X\} \sim \mathcal{N}(0, P_r)$, $\Im\{X\} \sim \mathcal{N}(0, P_i)$ with $P = P_r + P_i$.

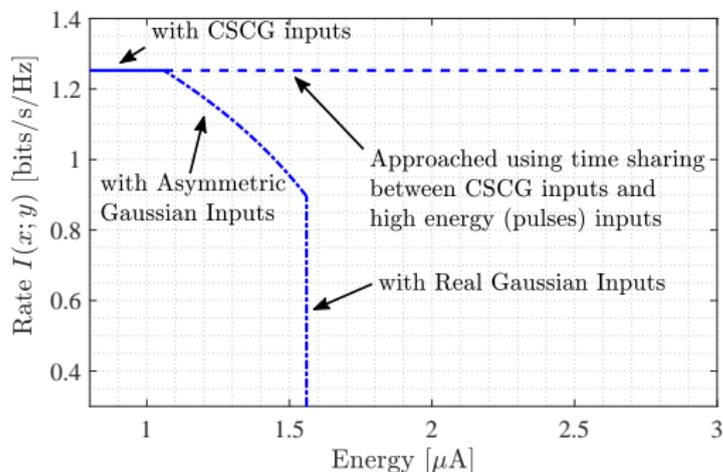


Observation

- 1 As a consequence of the nonlinearity, there exists a **non-trivial tradeoff** between rate and energy even in frequency-flat AWGN channel
- 2 Tradeoff-characterizing input distribution is **Gaussian with mean zero** and with **asymmetric power allocations to the real and imaginary dimensions**

Characterizing Fundamental Limits of SWIPT

Optimal inputs:



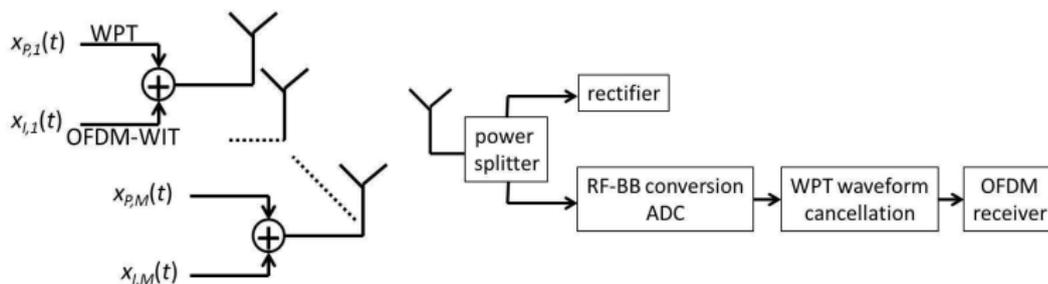
Observation

- 1 *Due to the nonlinearity, R-E tradeoff is an unbounded rectangle!*
- 2 *The capacity can be achieved/approached with simple time sharing between CSCG and flash signaling!*
- 3 *Radically different from the linear model*

Characterizing Fundamental Limits of SWIPT

... in a multicarrier system over frequency-selective channel with **Nonlinear** EH

- **Key idea:** superimposed deterministic and modulated (CSCG) waveforms



- Energy is harvested from the information and the power waveform
- How to design WIPT waveform?

Rate-Energy Region and Waveform Design

SWIPT Waveform Parameters: $\mathbf{S}_P, \mathbf{S}_I, \Phi_P, \Phi_I, \rho$

Rate-Energy region

$$C_{R-DC}(P) \triangleq \left\{ (R, I_{DC}) : R \leq I(\mathbf{S}_I, \Phi_I, \rho), \right. \\ \left. I_{DC} \leq i_{out}(\mathbf{S}_P, \mathbf{S}_I, \Phi_P, \Phi_I, \rho), \frac{1}{2} [\|\mathbf{S}_I\|_F^2 + \|\mathbf{S}_P\|_F^2] \leq P \right\}.$$

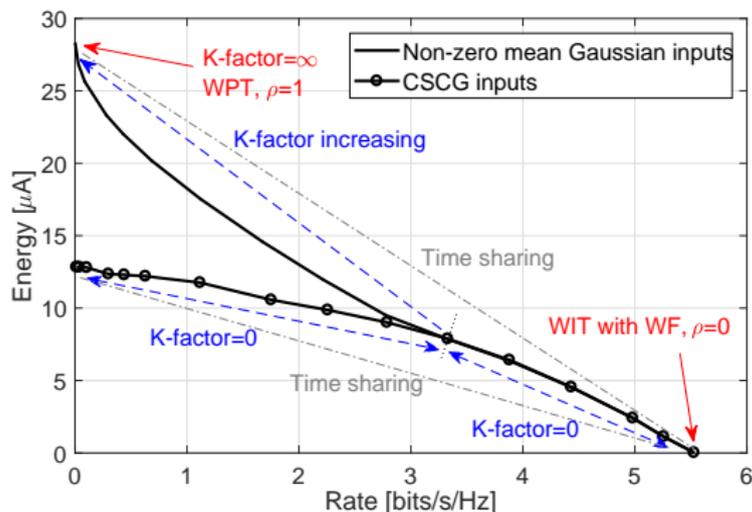
→ Find optimal values $\mathbf{S}_P^*, \mathbf{S}_I^*, \Phi_P^*, \Phi_I^*, \rho^*$ so as to enlarge C_{R-DC}

Energy maximization problem subject to the transmit power constraint and the rate constraint (being larger than a certain threshold \bar{R})

$$\begin{aligned} & \max_{\mathbf{S}_P, \mathbf{S}_I, \Phi_P, \Phi_I, \rho} && i_{out}(\mathbf{S}_P, \mathbf{S}_I, \Phi_P, \Phi_I, \rho) \\ & \text{subject to} && \frac{1}{2} [\|\mathbf{S}_I\|_F^2 + \|\mathbf{S}_P\|_F^2] \leq P, \\ & && I(\mathbf{S}_I, \Phi_I, \rho) \geq \bar{R}. \end{aligned}$$

Nonlinearity Changes The Whole Signal Design

Average Rx power of -20dBm. 20dB SNR. $B = 1\text{MHz}$. $N = 16$, $M = 1$.



Observation

- 1 Superposition of power and communication waveforms beneficial
- 2 A combination of PS and TS in general the best strategy
- 3 **Non-zero mean Gaussian input distribution outperforms zero-mean Gaussian input distribution!**

Communications and signals for WPT/WIPT systems

- Lay the foundations and tackle the challenges of the envisioned network
- Establish a **link** and **system-level design** inspired by communication theoretic ideas
- Develop a **signal theory** for transmission over the **nonlinear wireless power channel** and the linear wireless communication channel
- Identify the fundamental **tradeoff** between conveying information and power wirelessly

Nonlinearity is a fundamental property of the rectifier and is **beneficial**

- The wireless power channel is nonlinear
- **Do not compensate the nonlinearity but exploit it**
- Importance of accounting for the nonlinearity in any design involving wireless power
- Leads to **fundamental changes to WIPT design** (PHY and MAC layers)

Need for **bridging RF and comms/signal processing**

Communications and Signals Design for WPT

Y. Zeng, B. Clerckx and R. Zhang, "Communications and Signals Design for Wireless Power Transmission," IEEE Trans. on Comm, invited paper, Vol 65, No 5, pp 2264 - 2290, May 2017.

Systematic waveform designs for WPT

B. Clerckx and E. Bayguzina, "Waveform Design for Wireless Power Transfer," IEEE Trans on Sig Proc, Vol. 64, No. 23, pp. 6313-6328, Dec 2016.

Low-complexity design of WPT waveform

B. Clerckx and E. Bayguzina, "A Low-Complexity Multisine Waveform Design for Wireless Power Transfer," IEEE Antennas and Wireless Propagation Letters, vol 16, pp 2207 - 2210, 2017.

Large scale design for WPT waveforms

Y. Huang and B. Clerckx, "Large-Scale Multi-Antenna Multi-Sine Wireless Power Transfer," IEEE Trans. on Sig Proc., vol. 65, no. 21, pp 5812-5827, Nov 2017.

CSI feedback/acquisition in WPT

Y. Huang and B. Clerckx, "Waveform Design for Wireless Power Transfer with Limited Feedback," IEEE Trans. on Wireless Commun., vol 17, no 1, pp 415 - 429, Jan. 2018.

Transmit Diversity for WPT

B. Clerckx and J. Kim, "On the Beneficial Roles of Fading and Transmit Diversity in Wireless Power Transfer with Nonlinear Energy Harvesting," accepted to IEEE Trans. on Wireless Commun.

Prototyping and Experimentation of WPT

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Fundamentals of WIPT

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