

14: Power in AC Circuits

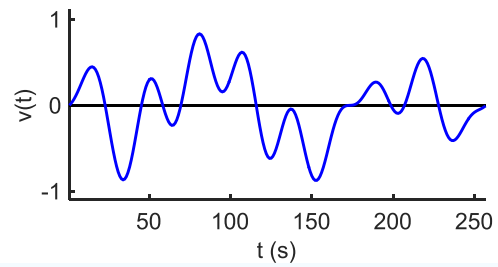
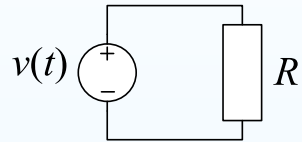
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- Cosine Wave RMS
- Power Factor +
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Average Power

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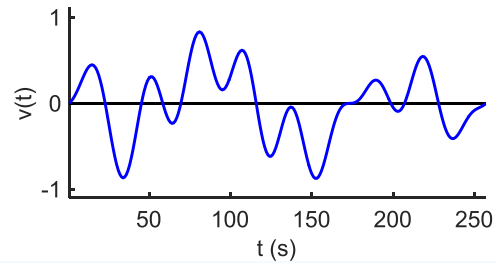
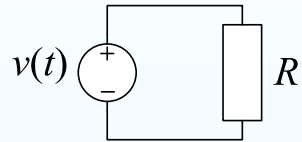
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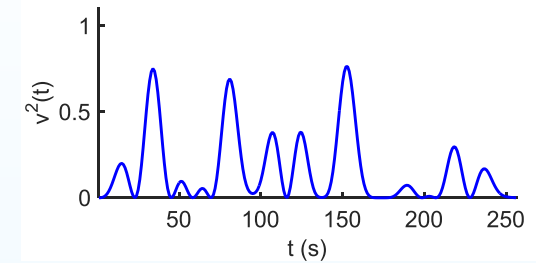
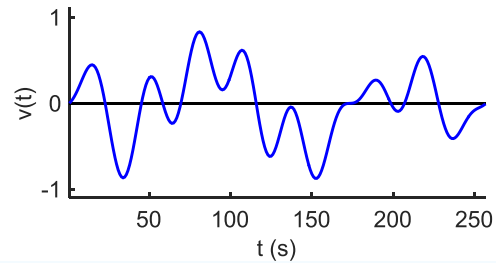
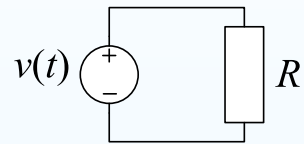


Instantaneous Power dissipated in R : $p(t) = \frac{v^2(t)}{R}$

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14: Power in AC Circuits

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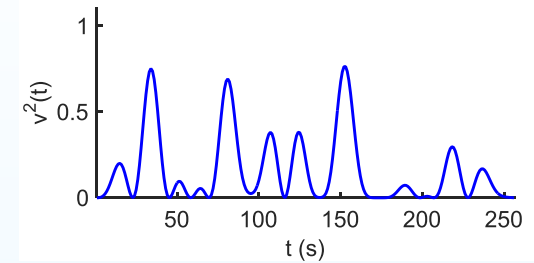
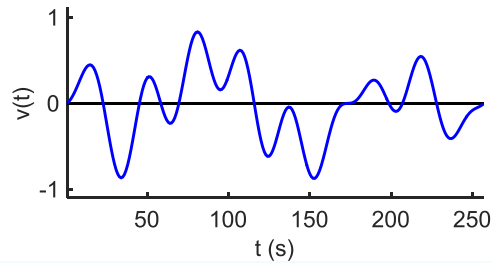
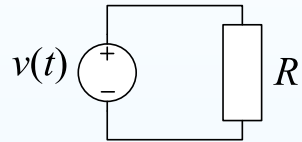


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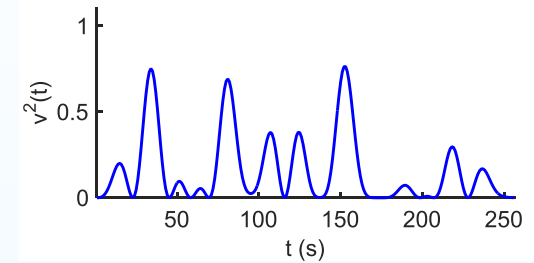
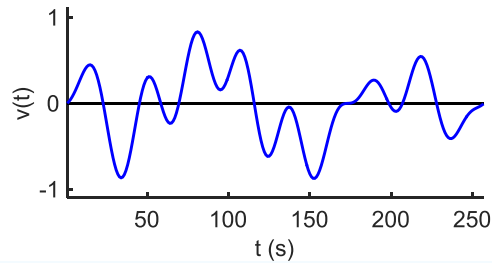
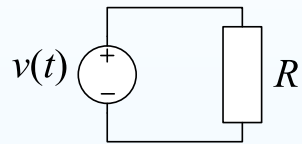
Average Power dissipated in R :

$$P = \frac{1}{T} \int_0^T p(t) dt$$

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14: Power in AC Circuits

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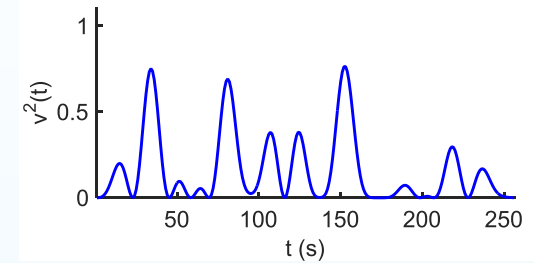
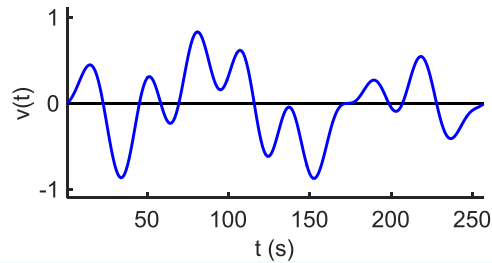
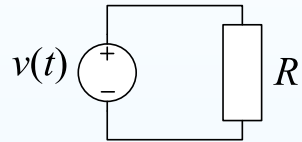
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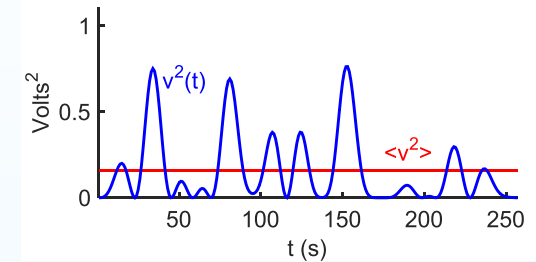
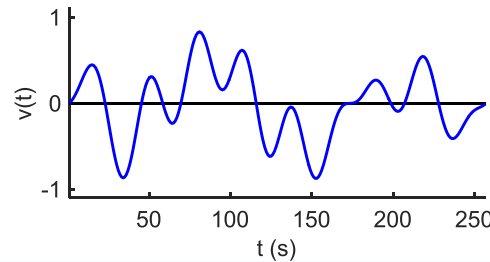
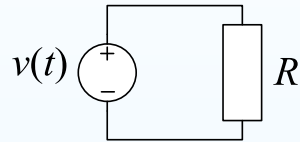
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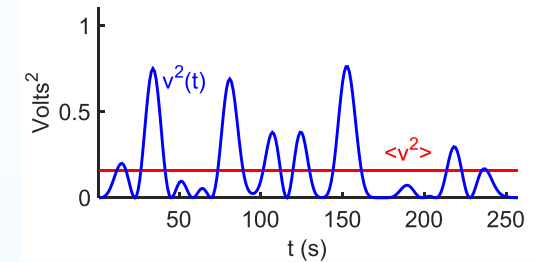
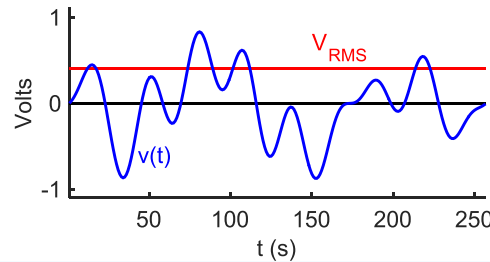
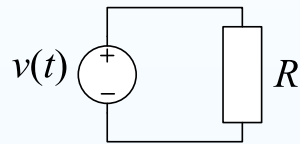
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$\langle v^2(t) \rangle$ is the value of $v^2(t)$ averaged over time

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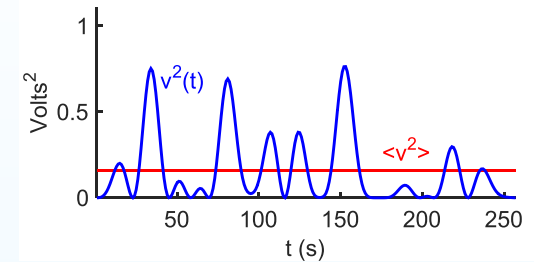
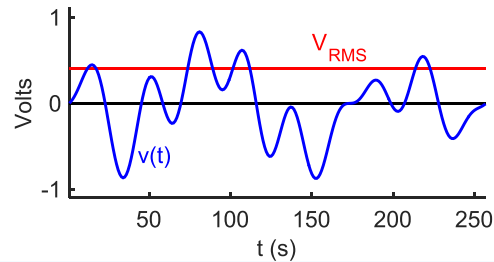
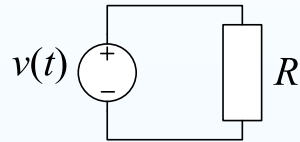
$\langle v^2(t) \rangle$ is the value of $v^2(t)$ averaged over time

We define the *RMS Voltage* (Root Mean Square): $V_{rms} \triangleq \sqrt{\langle v^2(t) \rangle}$

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14: Power in AC Circuits

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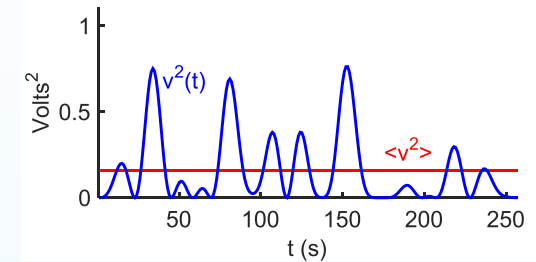
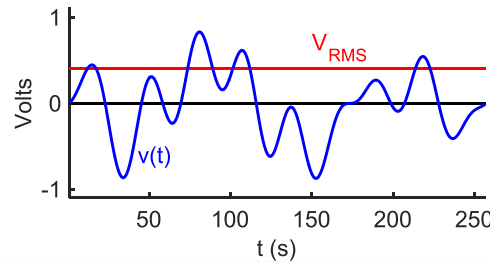
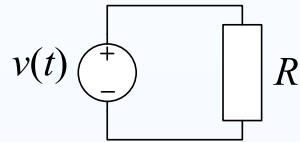
The average power dissipated in R is $P = \frac{\langle v^2(t) \rangle}{R} = \frac{(V_{rms})^2}{R}$

V_{rms} is the DC voltage that would cause R to dissipate the same power.

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14: Power in AC Circuits

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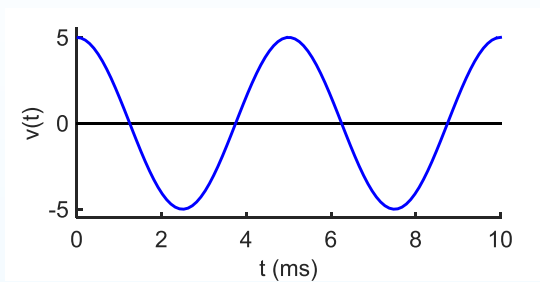
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We use *small letters* for time-varying voltages and *capital letters* for time-invariant values.

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- **Cosine Wave RMS**
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- Tellegen's Theorem
- Power Factor Correction
- Ideal Transformer
- Transformer Applications
- Summary

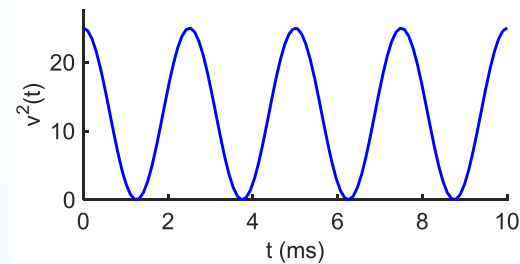
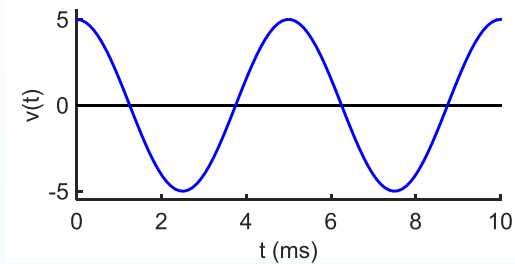


Cosine Wave: $v(t) = 5 \cos \omega t$. Amplitude is $V = 5 \text{ V}$.

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14: Power in AC Circuits

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- Summary



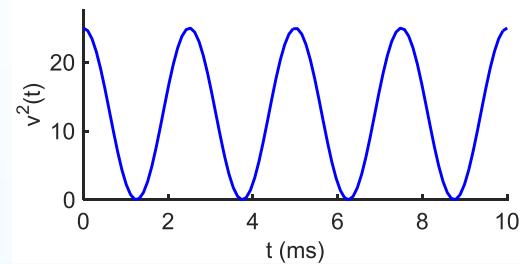
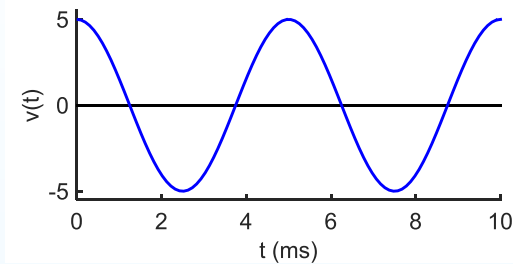
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Squared Voltage: $v^2(t) = V^2 \cos^2 \omega t = V^2 \left(\frac{1}{2} + \frac{1}{2} \cos 2\omega t \right)$

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14: Power in AC Circuits

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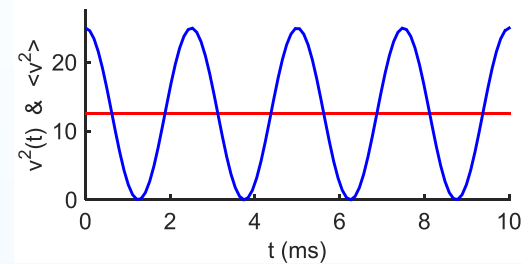
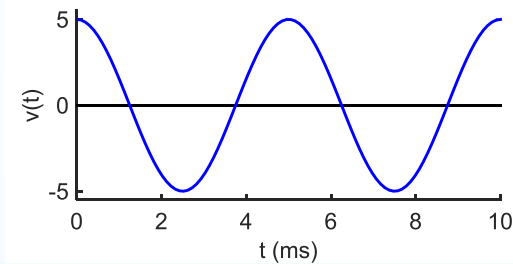
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14: Power in AC Circuits

- Average Power
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- Complex Power
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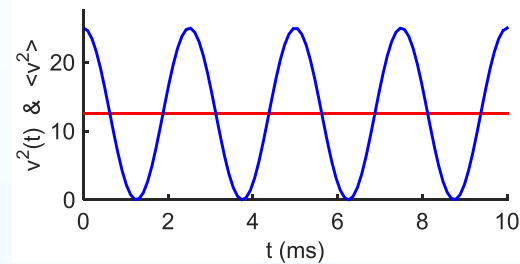
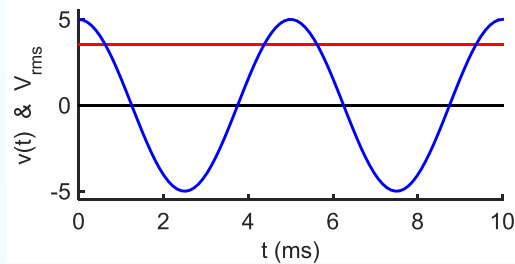
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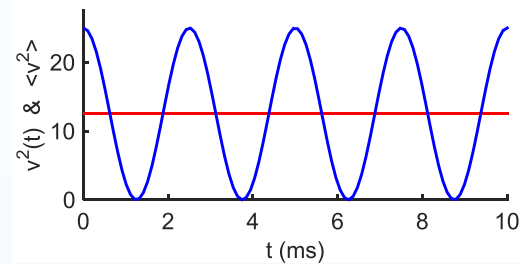
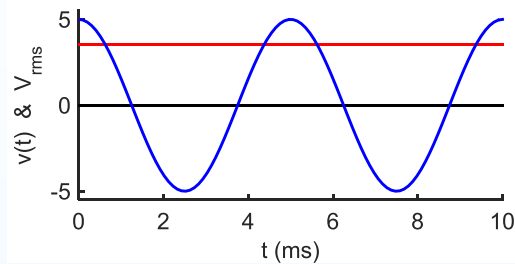
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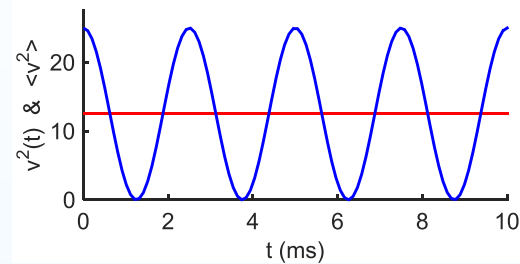
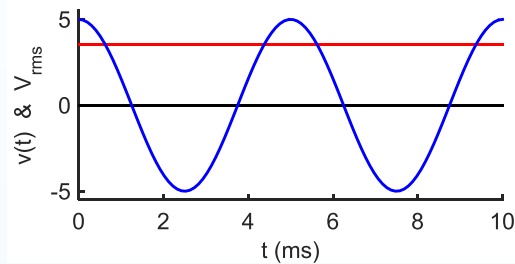
Note: Power engineers *always* use RMS voltages and currents exclusively and omit the “rms” subscript.

For example UK Mains voltage = 230 V rms = 325 V peak.

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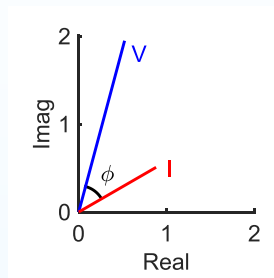
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In this lecture course only, a \sim overbar means $\div \sqrt{2}$: thus $\tilde{V} = \frac{1}{\sqrt{2}} V$.

Power Factor

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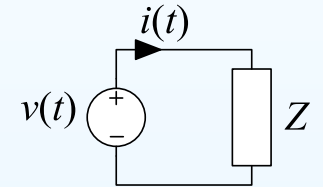
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$$V = |V| e^{j\theta_V}$$

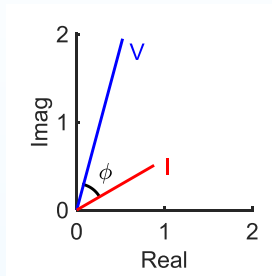
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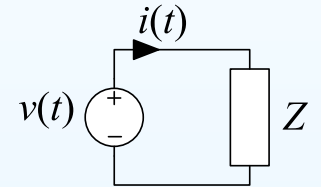
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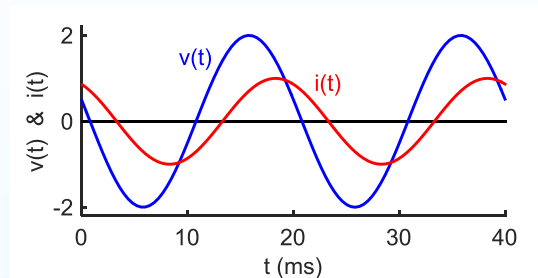
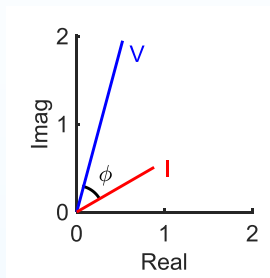
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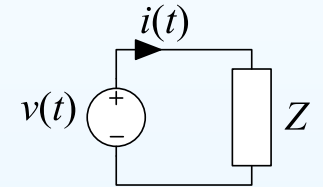
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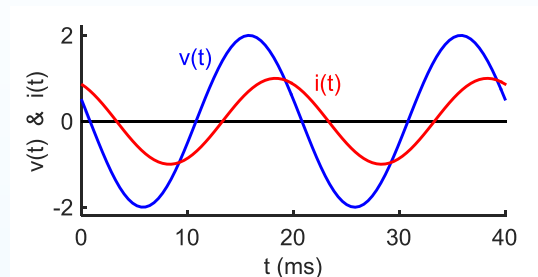
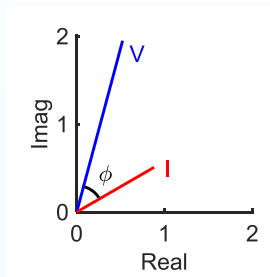
$$I = |I| e^{j\theta_I} \Leftrightarrow i(t) = |I| \cos(\omega t + \theta_I)$$



Power Factor

14: Power in AC Circuits

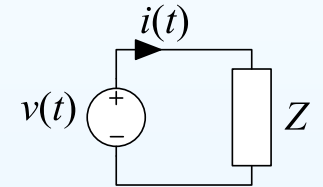
- Average Power
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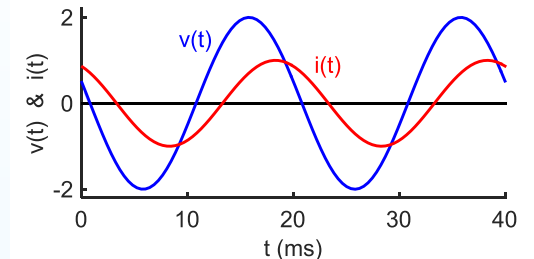
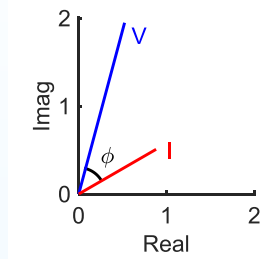
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Power Factor

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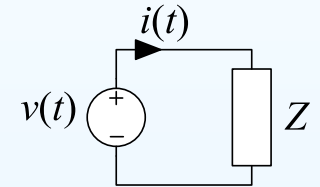
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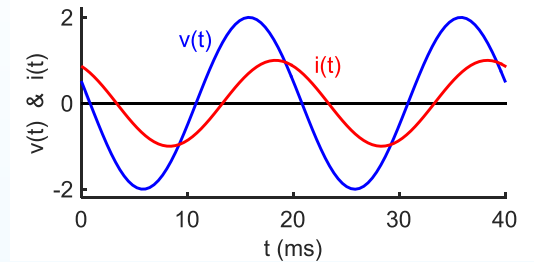
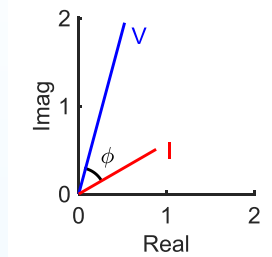
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Power Factor

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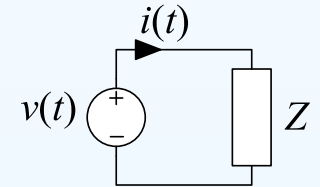
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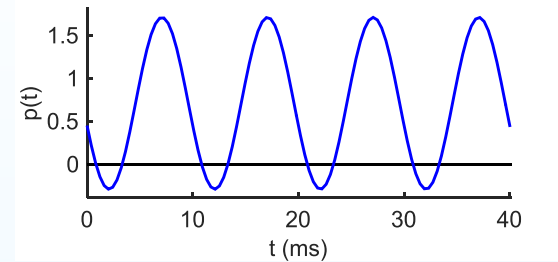
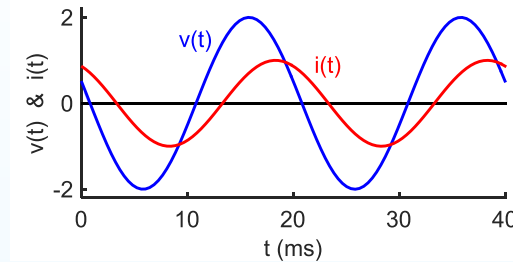
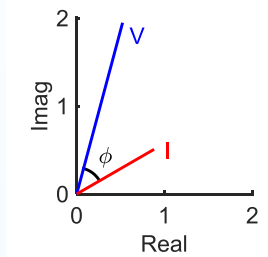
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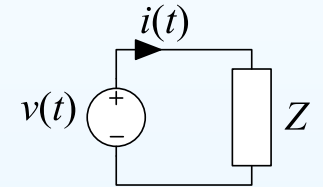
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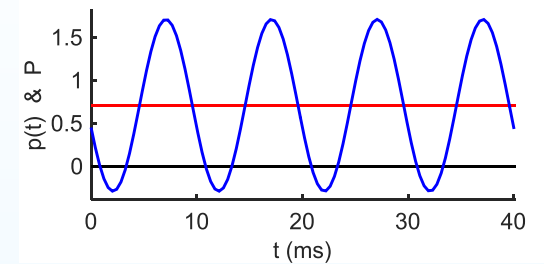
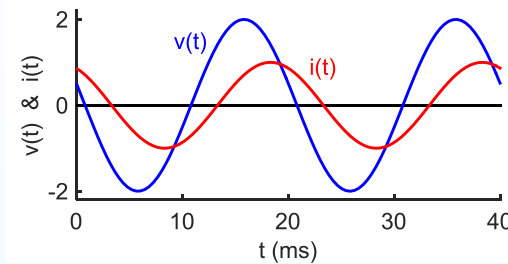
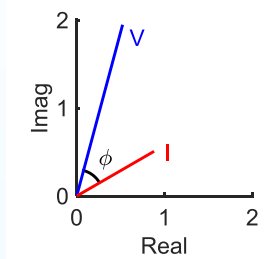
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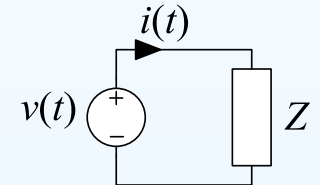
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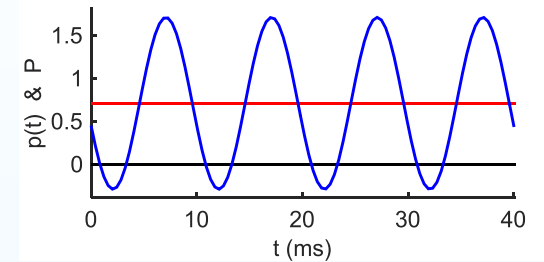
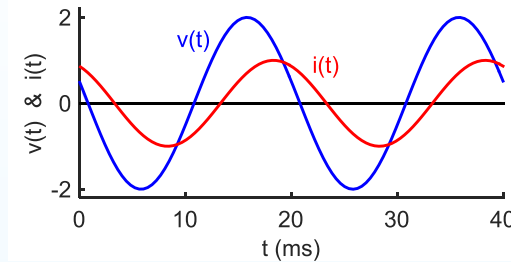
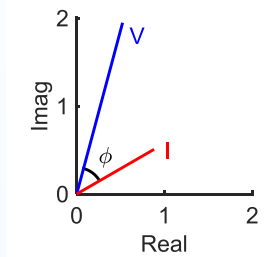
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Power Factor

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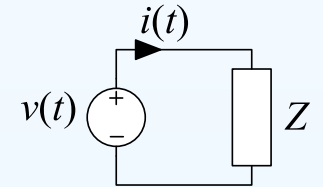
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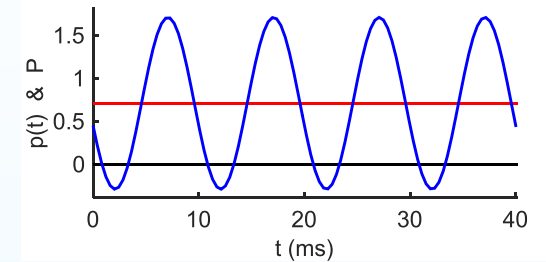
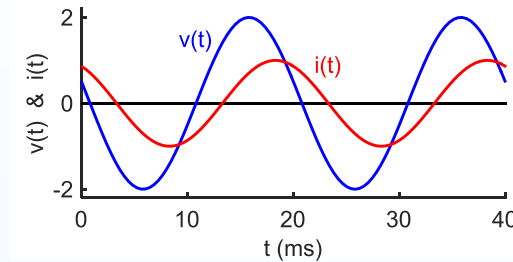
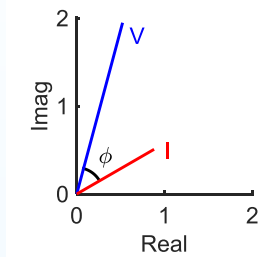
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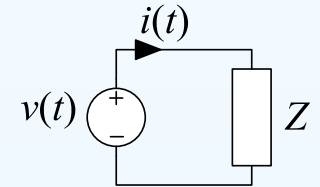
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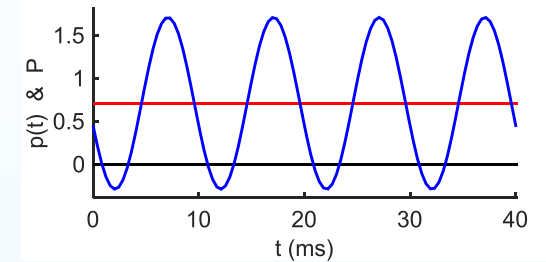
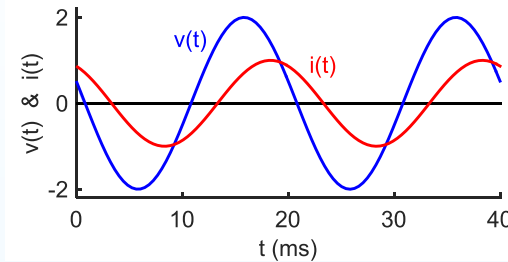
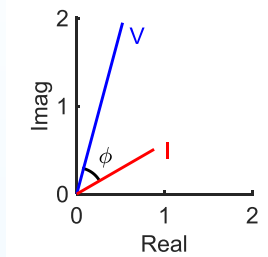
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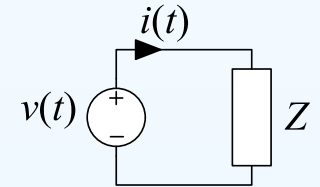
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$\phi > 0 \Leftrightarrow$ a *lagging power factor* (normal case: Current lags Voltage)

$\phi < 0 \Leftrightarrow$ a *leading power factor* (rare case: Current leads Voltage)

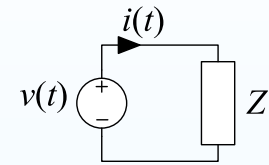
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where * means complex conjugate.



Complex Power

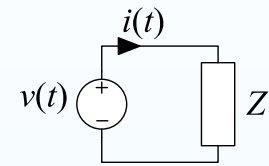
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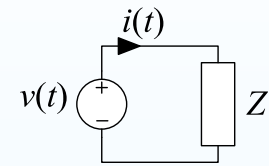
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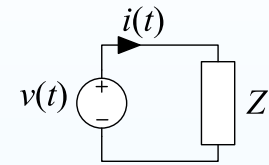
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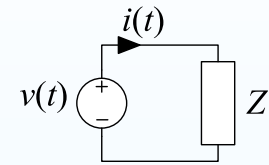
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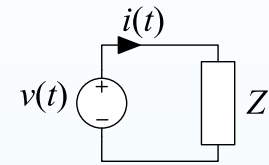
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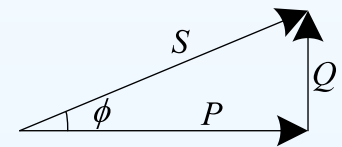
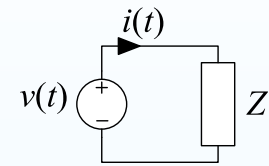
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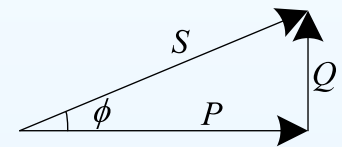
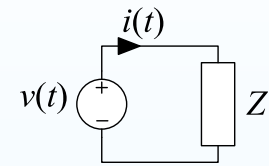
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Complex Power: $S \triangleq \tilde{V} \tilde{I}^* = P + jQ$ measured in **Volt-Amps (VA)**



Complex Power

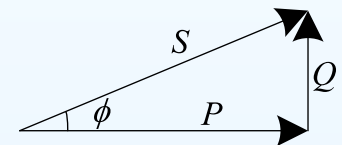
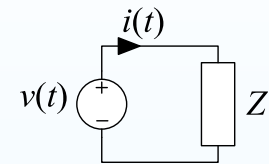
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Complex Power

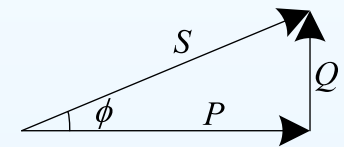
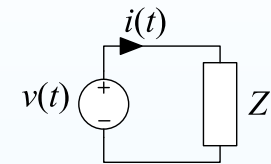
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Complex Power

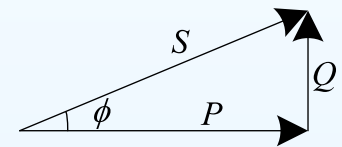
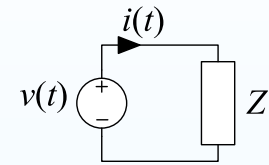
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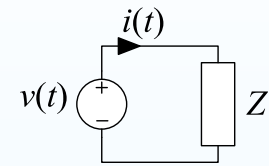
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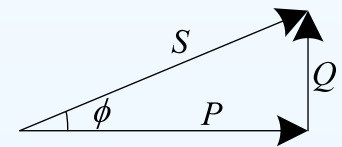
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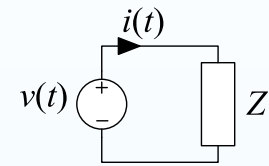
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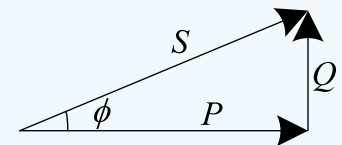
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Machines and transformers have capacity limits and power losses that are independent of $\cos \phi$; their ratings are always given in **apparent power**.

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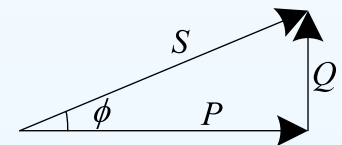
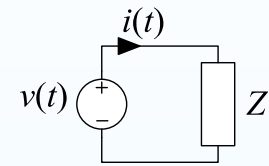
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Power Company: Costs \propto apparent power, Revenue \propto average power.

Power in R, L, C

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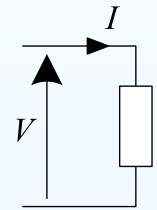
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Absorbs average power, no VARs ($Q = 0$)



Power in R, L, C

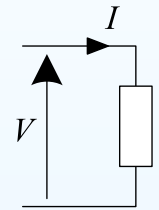
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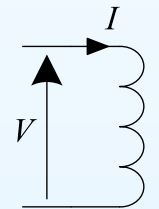
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Inductor: $S = j |\tilde{I}|^2 \omega L = j \frac{|\tilde{V}|^2}{\omega L} \quad \phi = +90^\circ$

No average power, **Absorbs VARs** ($Q > 0$)



Power in R, L, C

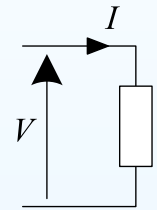
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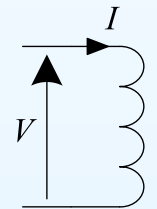
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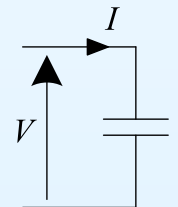
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No average power, **Generates VARs** ($Q < 0$)



Power in R, L, C

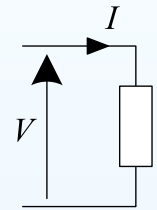
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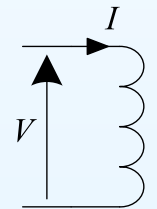
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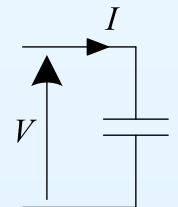
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VARs are **generated** by capacitors and **absorbed** by inductors

Power in R, L, C

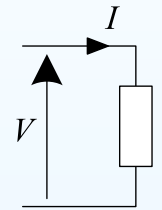
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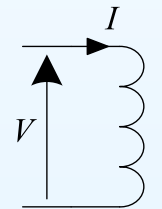
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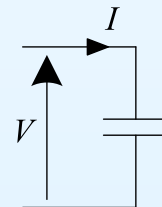
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The phase, ϕ , of the absorbed power, S , equals the phase of Z

Tellegen's Theorem

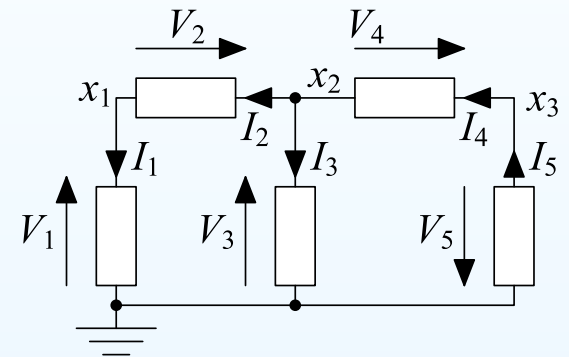
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Tellegen's Theorem: The complex power, S , dissipated in any circuit's components sums to zero.

x_n = voltage at node n

V_b, I_b = voltage/current in branch b
(obeying passive sign convention)



Tellegen's Theorem

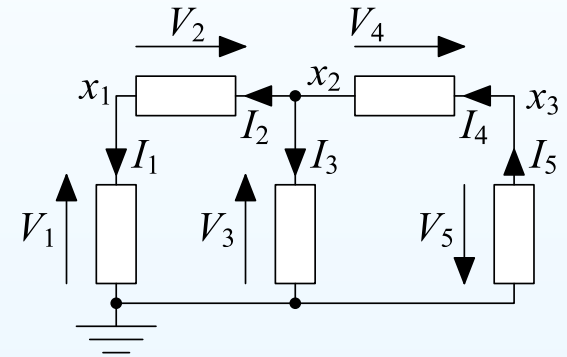
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branches (b)	nodes (n)		
	a_{b1}	a_{b2}	a_{b3}
1	1	0	0
2	-1	1	0
3	0	1	0
4	0	-1	1
5	0	0	-1

Tellegen's Theorem

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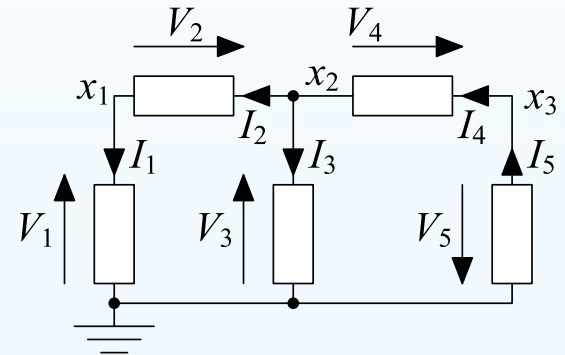
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e.g. branch 4 goes from 2 to 3 $\Rightarrow a_{4*} = [0, -1, 1]$



	nodes (n)		
a_{bn}	1	2	3
1	1	0	0
2	-1	1	0
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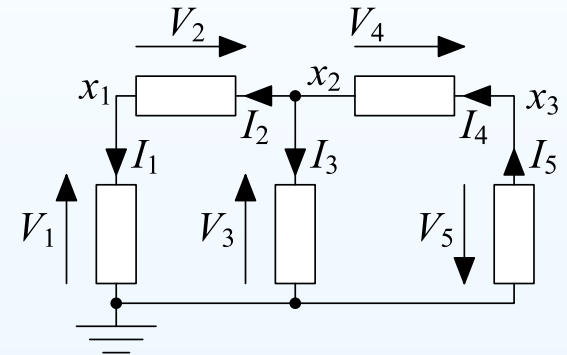
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$$a_{bn} \triangleq \begin{cases} -1 & \text{if } V_b \text{ starts from node } n \\ +1 & \text{if } V_b \text{ ends at node } n \\ 0 & \text{else} \end{cases}$$

e.g. branch 4 goes from 2 to 3 $\Rightarrow a_{4*} = [0, -1, 1]$

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Tellegen's Theorem

14: Power in AC Circuits

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Tellegen's Theorem: The complex power, S , dissipated in any circuit's components sums to zero.

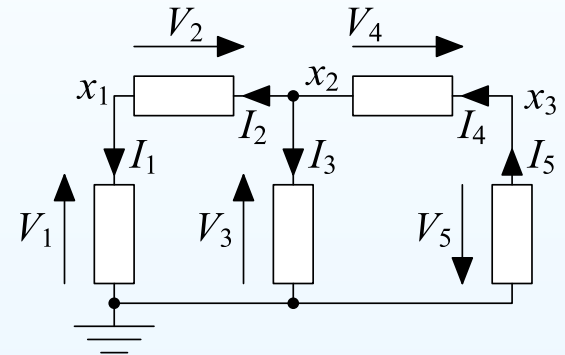
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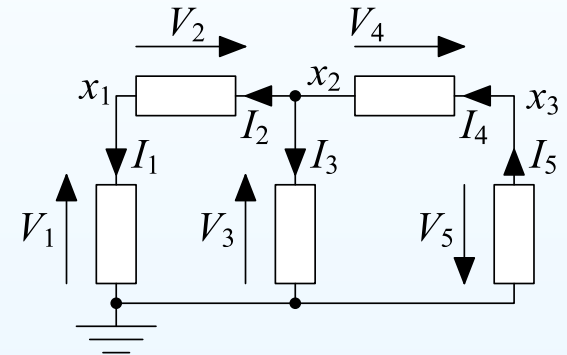
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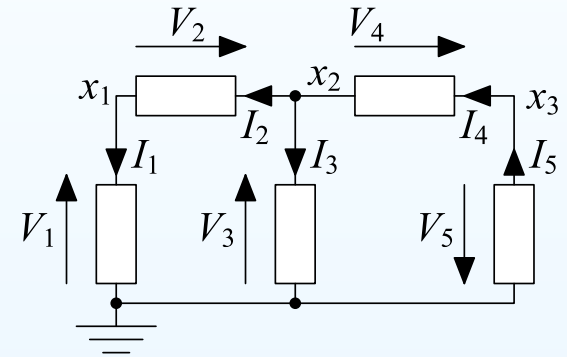
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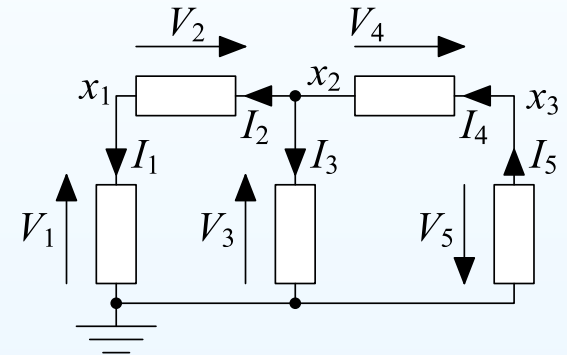
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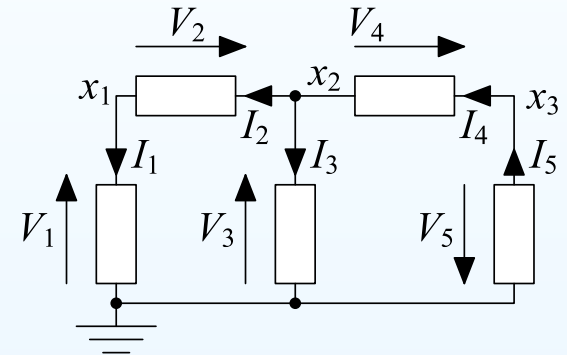
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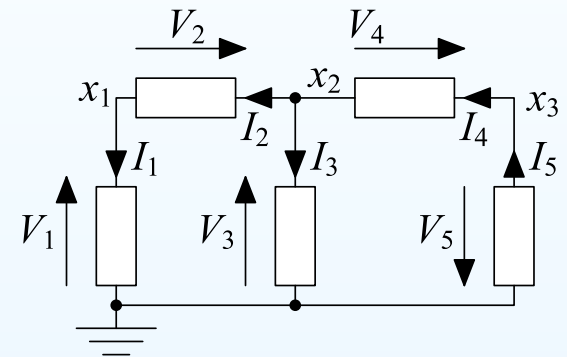
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Note: $\sum_b S_b = 0 \Rightarrow \sum_b P_b = 0$ and also $\sum_b Q_b = 0$.

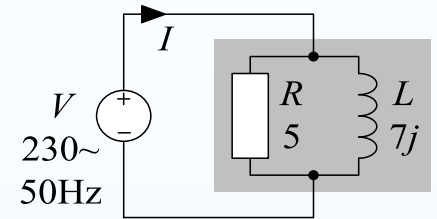
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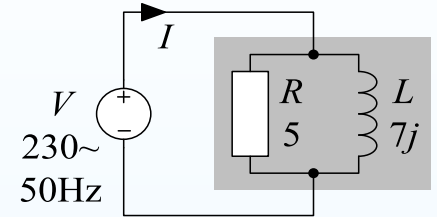


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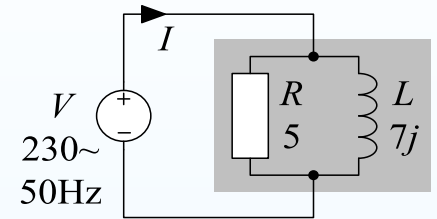
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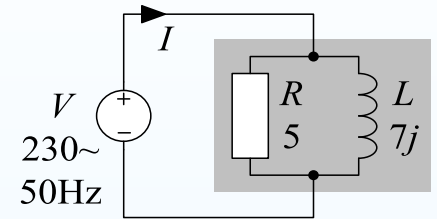
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Power Factor Correction

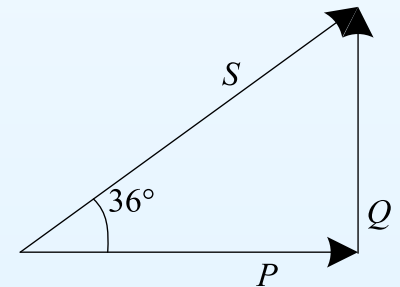
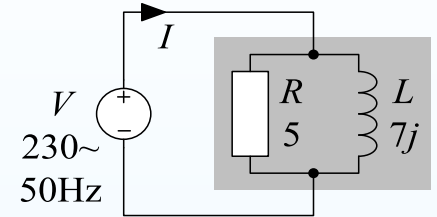
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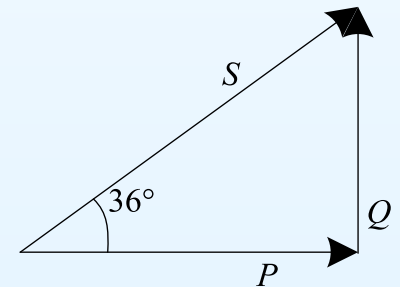
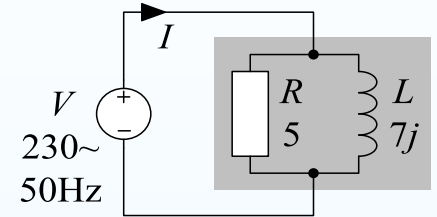
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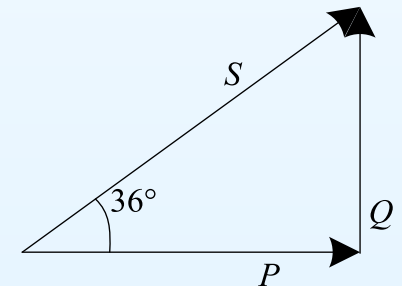
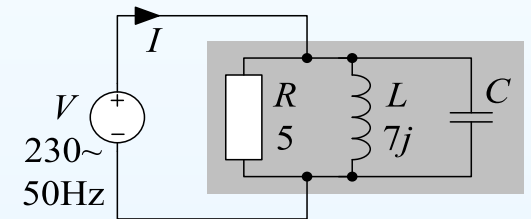
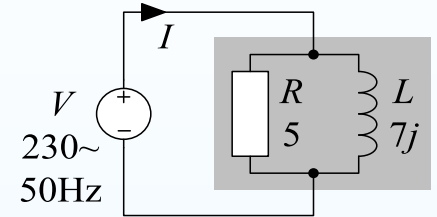
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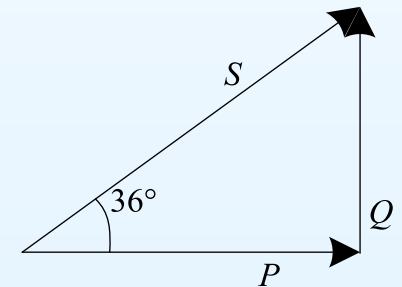
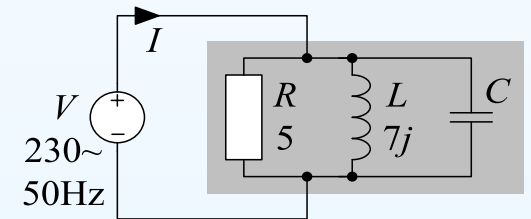
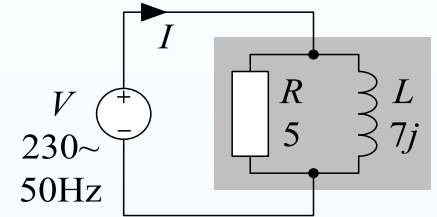
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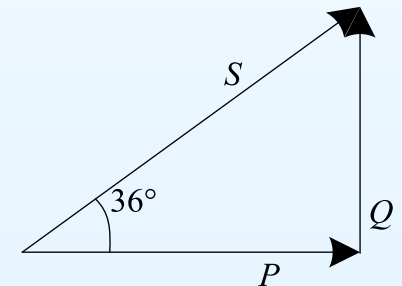
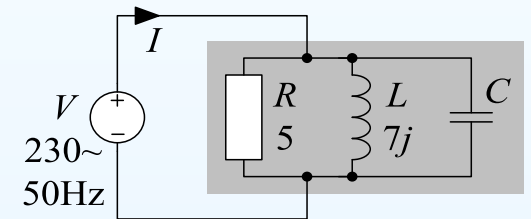
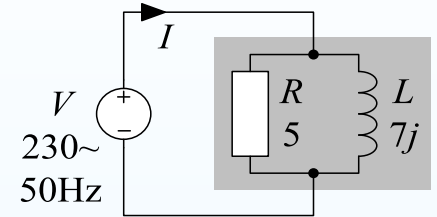
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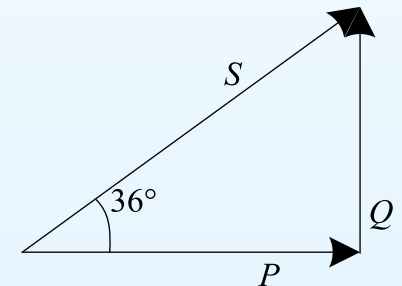
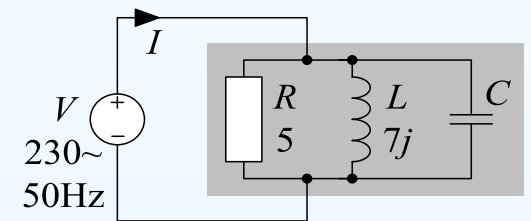
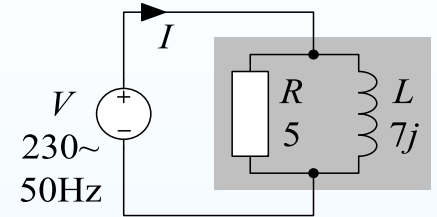
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Power Factor Correction

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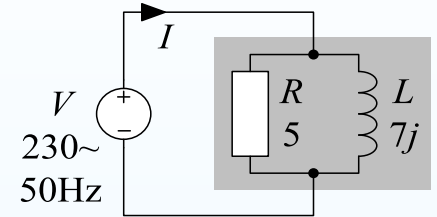
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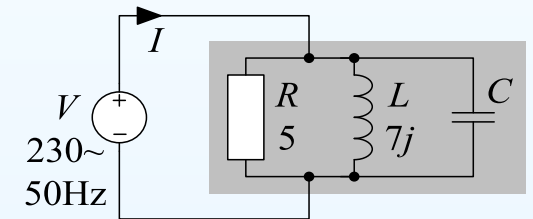
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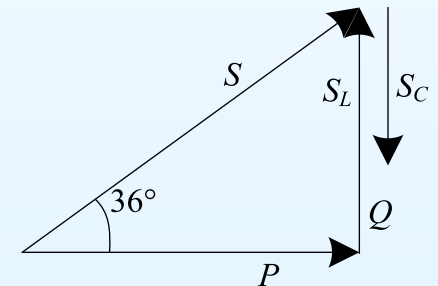
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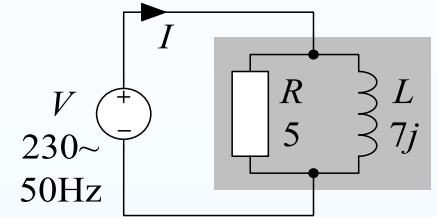
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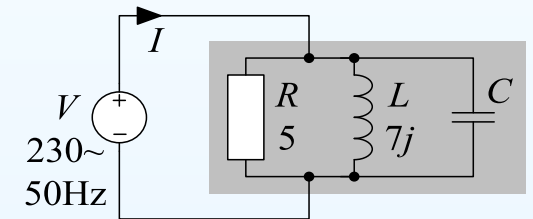
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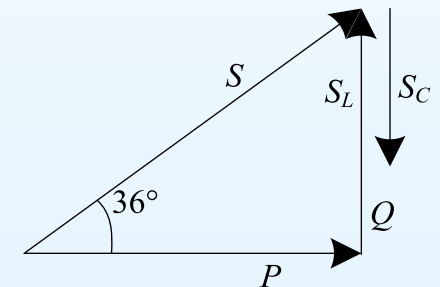
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Power Factor Correction

14: Power in AC Circuits

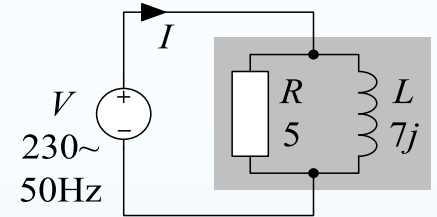
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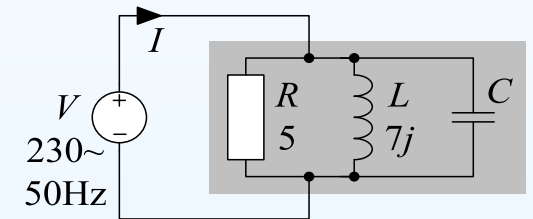
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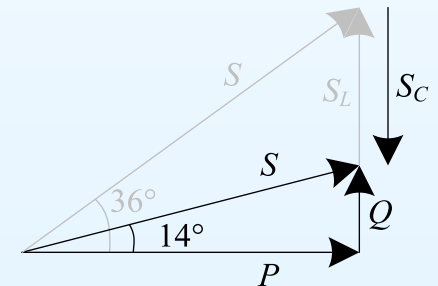
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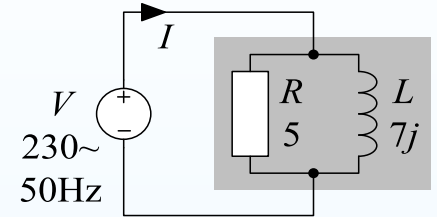
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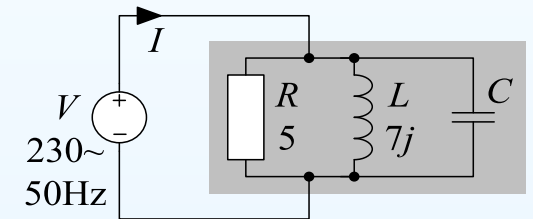
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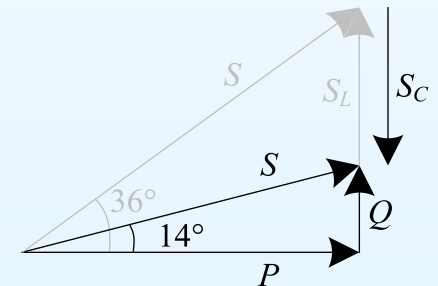
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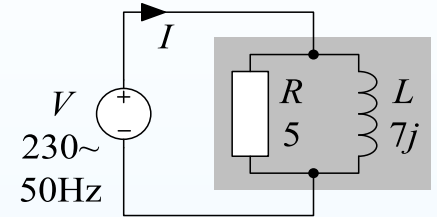
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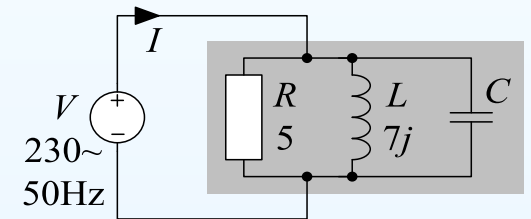
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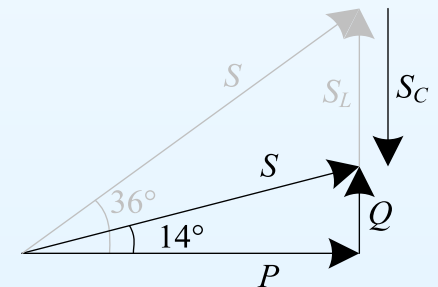
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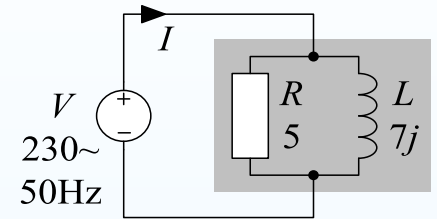
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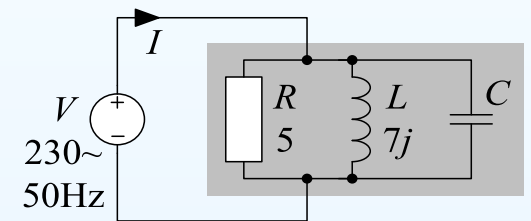
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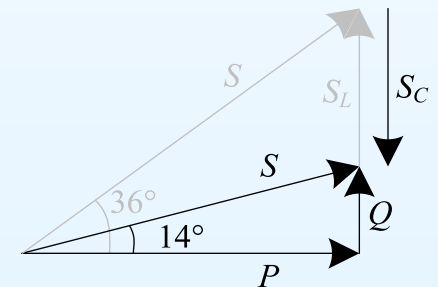
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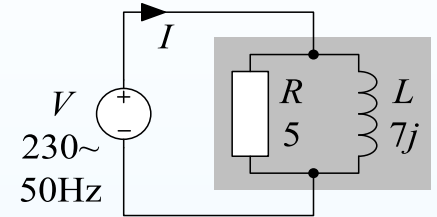
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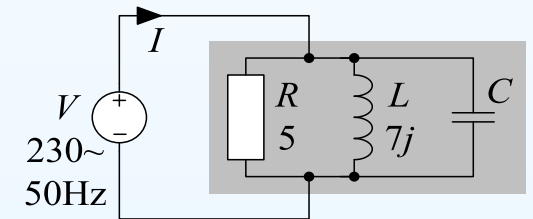
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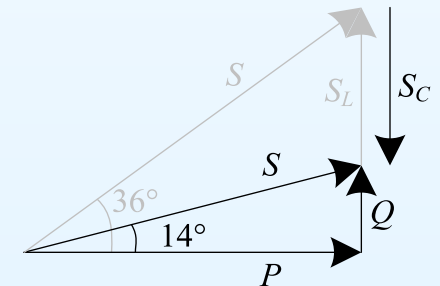
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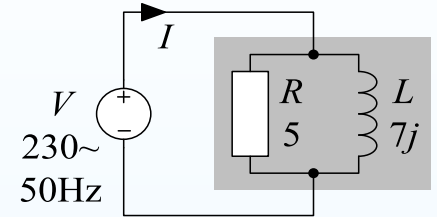
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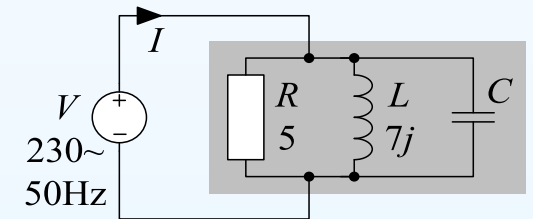
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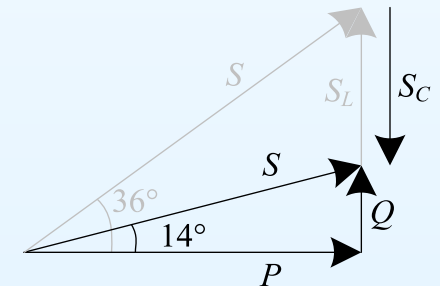
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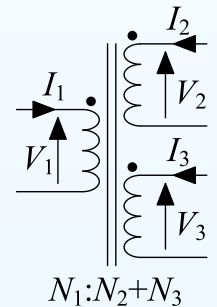
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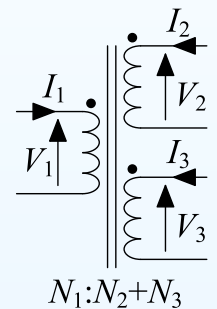
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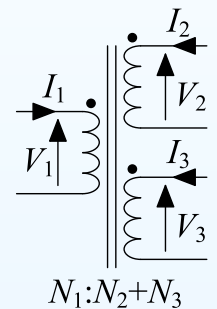
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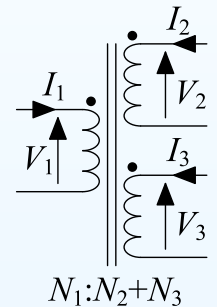
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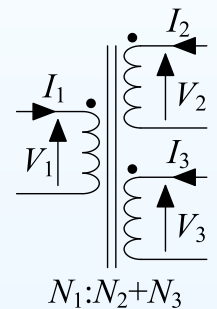
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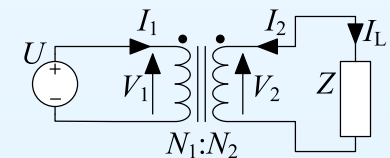
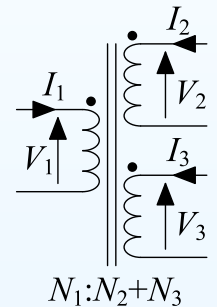
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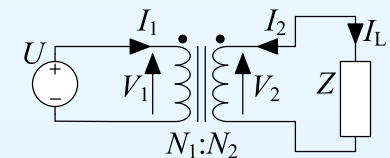
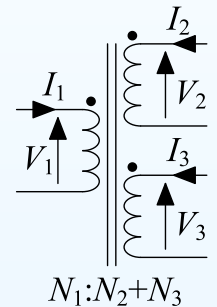
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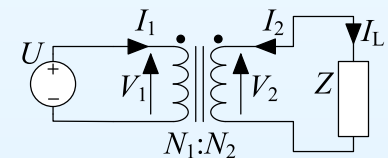
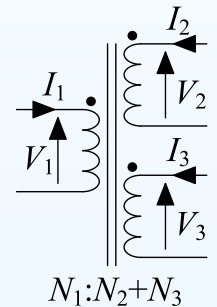
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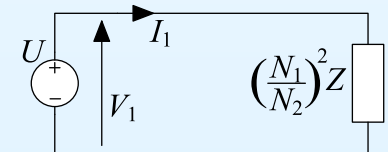
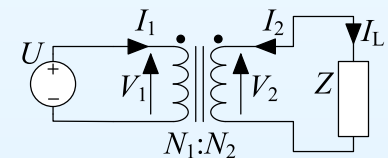
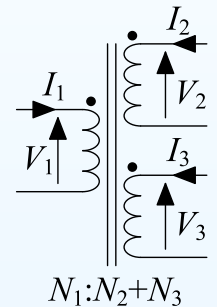
Special Case:

For a 2-winding transformer this simplifies to

$$V_2 = \frac{N_2}{N_1} V_1 \text{ and } I_L = -I_2 = \frac{N_1}{N_2} I_1$$

$$\text{Hence } \frac{V_1}{I_1} = \left(\frac{N_1}{N_2}\right)^2 \frac{V_2}{I_L} = \left(\frac{N_1}{N_2}\right)^2 Z$$

Equivalent to a *reflected impedance* of $\left(\frac{N_1}{N_2}\right)^2 Z$



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$$100 \text{ kVA@ } 1 \text{ kV} = 100 \text{ A} \Rightarrow \tilde{I}^2 R = 10 \text{ kW losses.}$$

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Electronic equipment requires $\leq 20 \text{ V}$ but mains voltage is $240 \text{ V} \sim$.

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Microphone on long cable is susceptible to interference from nearby mains cables. An $N : 1$ transformer reduces the microphone voltage by N but reduces interference by N^2 .

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Isolation

There is no electrical connection between the windings of a transformer so circuitry (or people) on one side will not be endangered by a failure that results in high voltages on the other side.

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For further details see Hayt Ch 11 or Irwin Ch 9.