

Revision Lecture 1: Nodal
Analysis &
Frequency Responses

- Exam
- Nodal Analysis
- Op Amps
- Block Diagrams
- Diodes
- Reactive Components
- Phasors
- Plotting Frequency Responses
- LF and HF Asymptotes
- Corner frequencies (linear factors)
- Sketching Magnitude Responses (linear factors)
- Filters
- Resonance

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Exam

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Exam Format

Question 1 (40%): eight short parts covering the whole syllabus.

Questions 2 and 3: single topic questions (answer both)

Syllabus

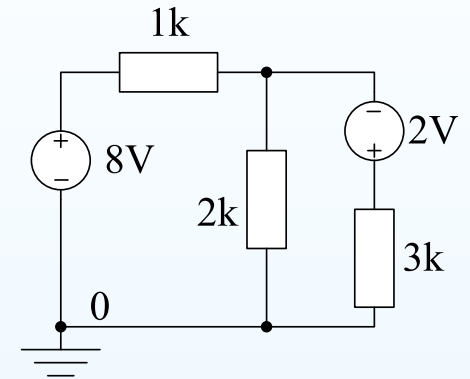
Does include: Everything in the notes.

Does not include: Two-port parameters (2008:1j), Gaussian elimination (2007:2c), Application areas (2008:3d), Nullators and Norators (2008:4c), Small-signal component models (2008:4e), Gain-bandwidth product (2006:4c), Zener Diodes (2008/9 syllabus), Non-ideal models of L, C and transformer (2011/12 syllabus), Transmission lines VSWR and crank diagram (2011/12 syllabus).

Nodal Analysis

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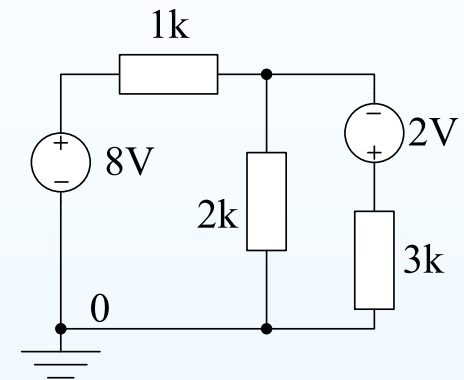


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(1) Pick reference node.



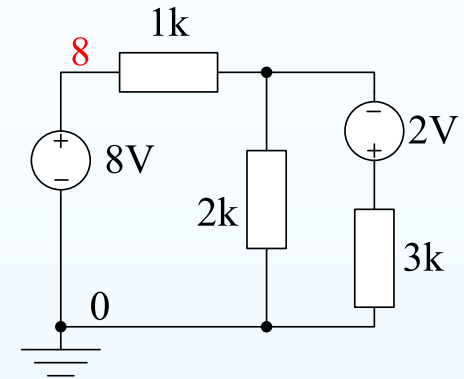
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(1) Pick reference node.

(2) Label nodes: 8

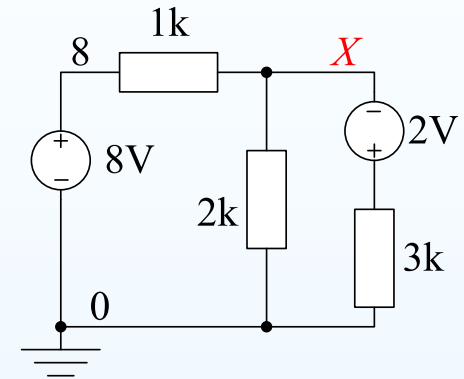


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- (1) Pick reference node.
- (2) Label nodes: 8 , X

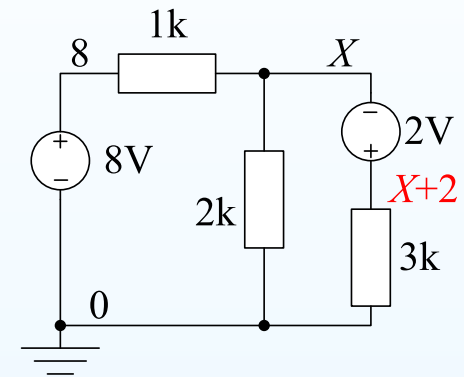


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- (2) Label nodes: 8 , X and $X + 2$ since it is joined to X via a voltage source.



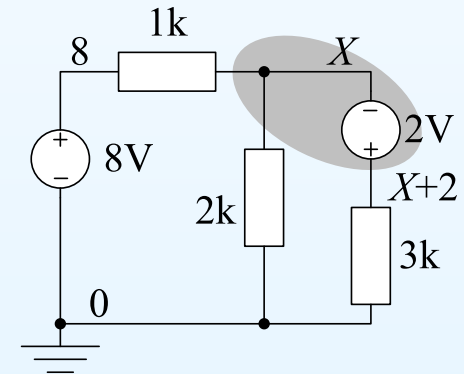
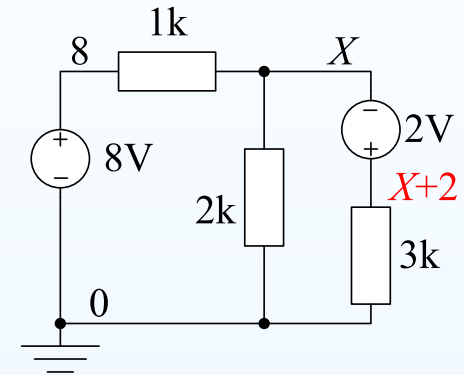
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- (2) Label nodes: 8 , X and $X + 2$ since it is joined to X via a voltage source.
- (3) Write KCL equations but count all the nodes connected via floating voltage sources as a single “super-node” giving one equation

$$\frac{X-8}{1} + \frac{X}{2} + \frac{(X+2)-0}{3} = 0$$



Nodal Analysis

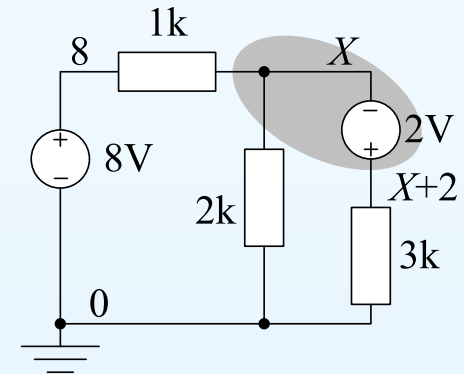
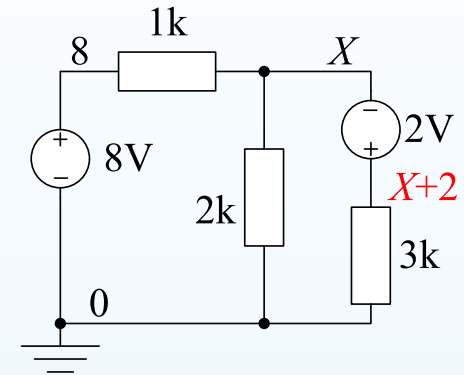
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Ohm's law always involves the difference between the voltages at **either end of a resistor**. (Obvious but easily forgotten)



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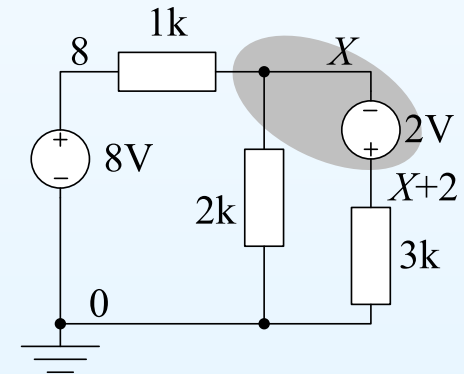
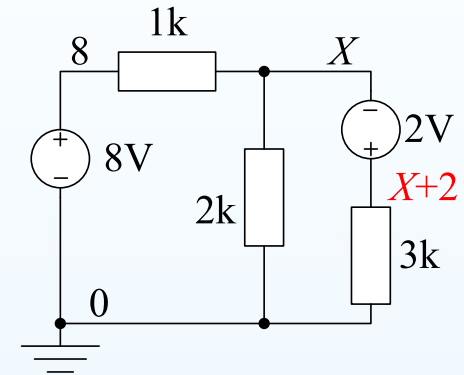
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- (4) Solve the equations: $X = 4$

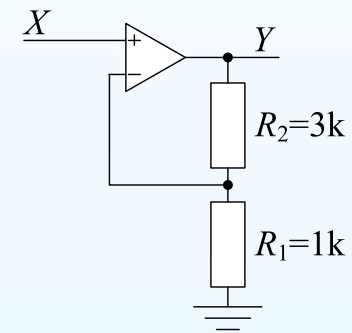


Op Amps

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- **Ideal Op Amp:** (a) Zero input current, (b) Infinite gain
(b) $\Rightarrow V_+ = V_-$ provided the circuit has **negative feedback**.
- **Negative Feedback:** An increase in V_{out} makes $(V_+ - V_-)$ decrease.



Op Amps

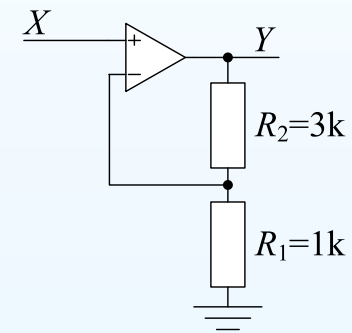
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Non-inverting amplifier

$$Y = \left(1 + \frac{3}{1}\right) X$$



Op Amps

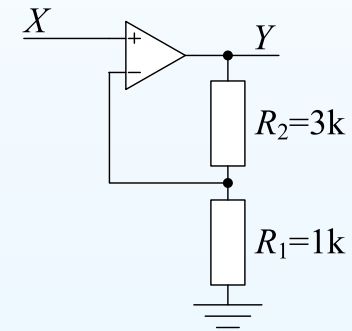
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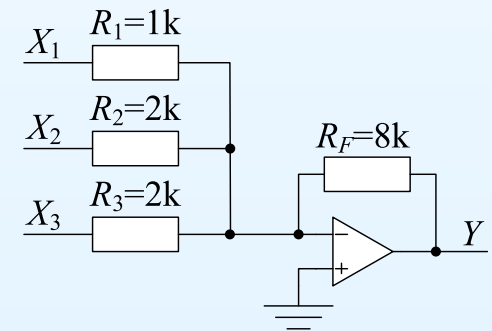
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$$Y = \left(1 + \frac{3}{1}\right) X$$



Inverting amplifier

$$Y = \frac{-8}{1} X_1 + \frac{-8}{2} X_2 + \frac{-8}{2} X_3$$



Op Amps

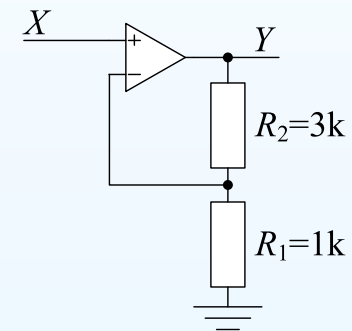
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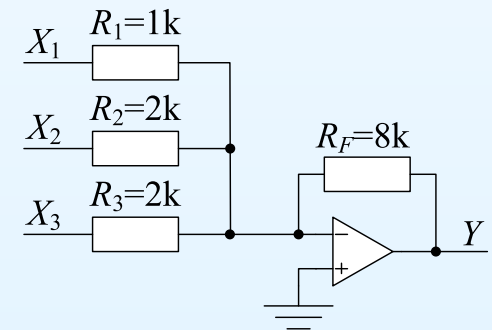
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Nodal Analysis: Use two separate KCL equations at V_+ and V_- .

Op Amps

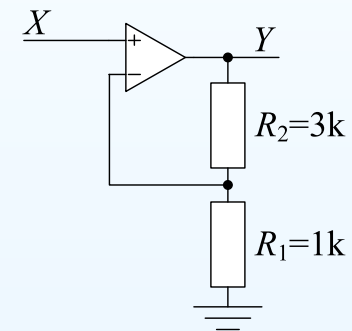
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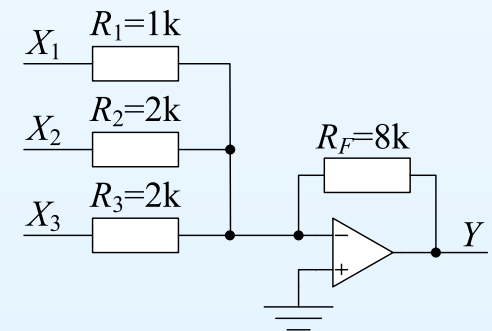
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Nodal Analysis: Use two separate KCL equations at V_+ and V_- .

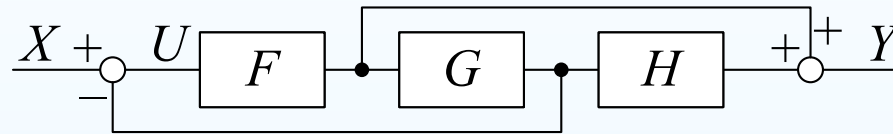
Do not do KCL at V_{out} except to find the op-amp output current.

Block Diagrams

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Blocks are labelled with their gains and connected using adder/subtractors shown as circles. Adder inputs are marked + for add or - for subtract.

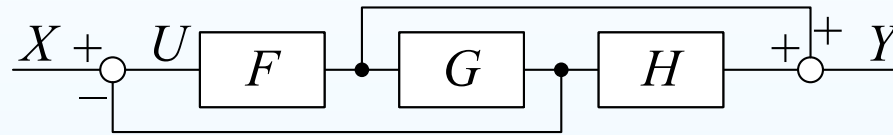


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To analyse:

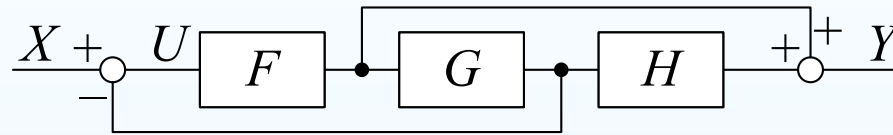
1. Label the inputs, the outputs and the output of each adder.

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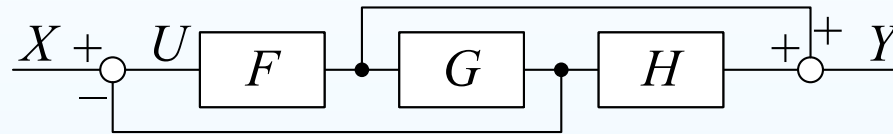
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2. Write down an equation for each variable:
 - $U = X - FGU$
 - Follow signals back through the blocks until you meet a labelled node.

Block Diagrams

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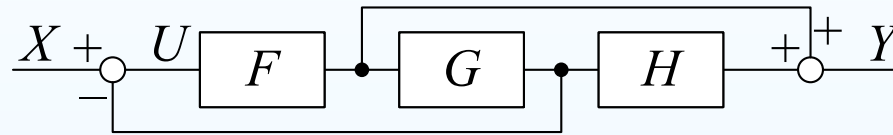
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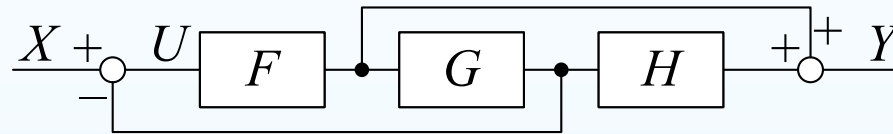
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3. Solve the equations (eliminate intermediate node variables):
 - $U(1 + FG) = X$

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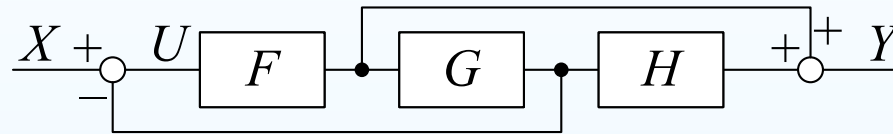
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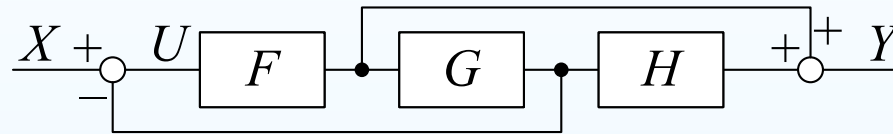
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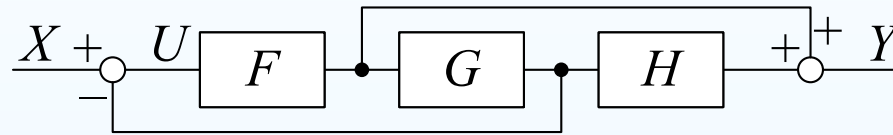
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3. Solve the equations (eliminate intermediate node variables):

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- $Y = (1 + GH)FU = \frac{(1+GH)F}{1+FG} X$

[Note: “Wires” carry information not current: KCL not valid]

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Each diode in a circuit is in one of two modes; each has an **equality** condition and an **inequality** condition:

- Off: $I_D = 0, V_D < 0.7$
- On: $V_D = 0.7, I_D > 0$

- (a) Guess the mode
- (b) Do nodal analysis assuming the equality condition
- (c) Check the inequality condition. If the inequality condition fails, you made the wrong guess.

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Each diode in a circuit is in one of two modes; each has an **equality** condition and an **inequality** condition:

- Off: $I_D = 0, V_D < 0.7 \Rightarrow$ Diode = open circuit
- On: $V_D = 0.7, I_D > 0$

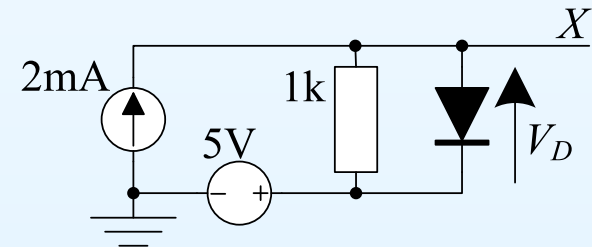
(a) Guess the mode

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- Assume Diode Off

$$X = 5 + 2 = 7$$



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Each diode in a circuit is in one of two modes; each has an **equality** condition and an **inequality** condition:

- Off: $I_D = 0, V_D < 0.7 \Rightarrow$ Diode = open circuit
- On: $V_D = 0.7, I_D > 0$

(a) Guess the mode

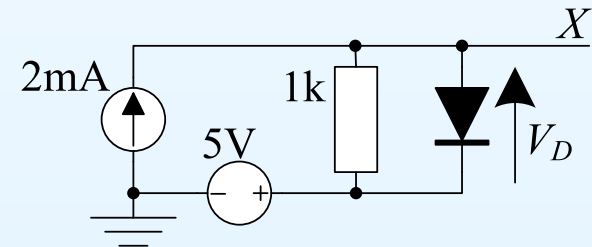
(b) Do nodal analysis assuming the equality condition

(c) Check the inequality condition. If the inequality condition fails, you made the wrong guess.

- Assume Diode Off

$$X = 5 + 2 = 7$$

$$V_D = 2$$



Diodes

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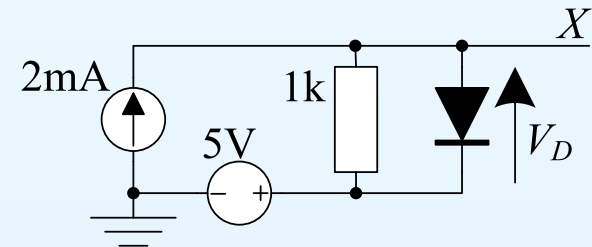
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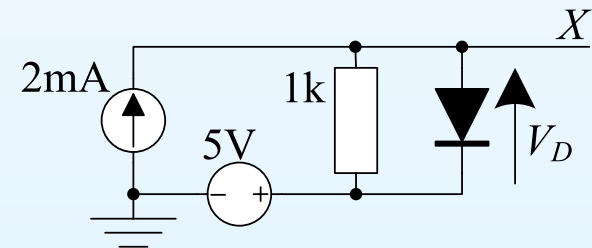
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Diodes

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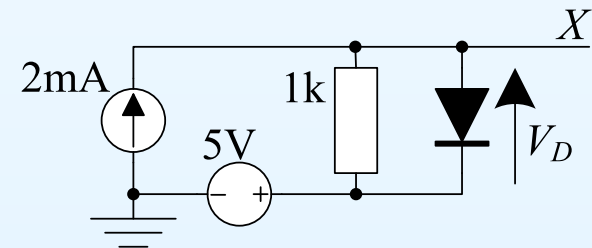
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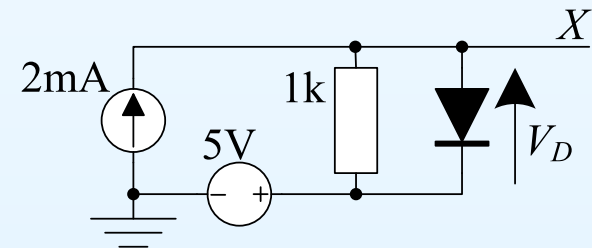
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$$X = 5 + 0.7 = 5.7$$

$$I_D + \frac{0.7}{1k} = 2 \text{ mA} \quad \text{OK: } I_D > 0$$



Reactive Components

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- **Impedances:** $R, j\omega L, \frac{1}{j\omega C} = \frac{-j}{\omega C}$.

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Reactive Components

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Phasors

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A phasor represents a time-varying sinusoidal waveform by a **fixed complex number**.

Waveform

$$x(t) = F \cos \omega t - G \sin \omega t$$

Phasor

$$X = F + jG$$

Phasors

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$$x(t) = A \cos (\omega t + \theta)$$

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$$X = Ae^{j\theta} = A\angle\theta$$

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Phasors

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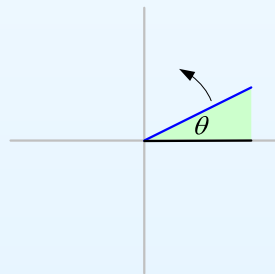
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$x(t)$ is the projection of a rotating rod onto the real (horizontal) axis.

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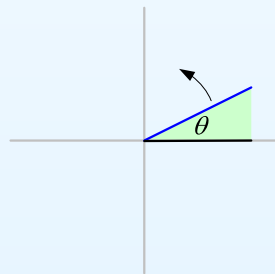
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$$\text{RMS Phasor: } \tilde{V} = \frac{1}{\sqrt{2}} V$$

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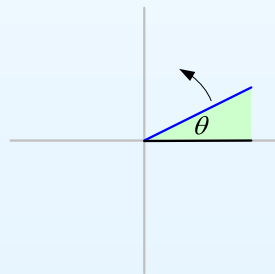
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Phasors

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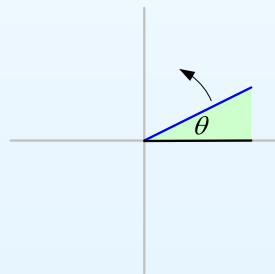
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$$\text{Complex Power: } \tilde{V} \tilde{I}^* = |\tilde{I}|^2 Z = \frac{|\tilde{V}|^2}{Z^*} = P + jQ$$

P is average power (Watts), Q is reactive power (VARs)

Plotting Frequency Responses

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Plotting Frequency Responses

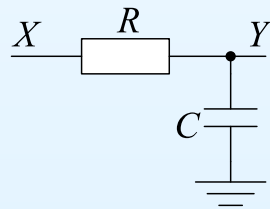
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Plotting Frequency Responses

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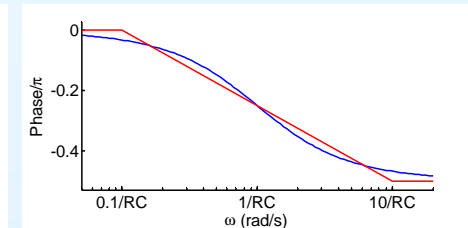
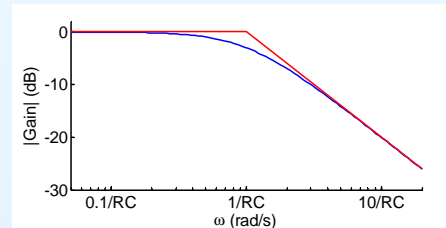
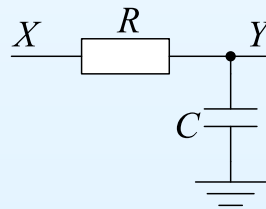
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$$\frac{Y}{X} = \frac{\frac{1}{j\omega C}}{R + \frac{1}{j\omega C}} = \frac{1}{j\omega RC + 1} = \frac{1}{\frac{j\omega}{\omega_c} + 1} \text{ where } \omega_c = \frac{1}{RC}$$

LF and HF Asymptotes

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- Frequency response is always a ratio of two polynomials in $j\omega$ with real coefficients that depend on the component values.
 - The terms with the **lowest** power of $j\omega$ on top and bottom gives the **low-frequency** asymptote
 - The terms with the **highest** power of $j\omega$ on top and bottom gives the **high-frequency** asymptote.

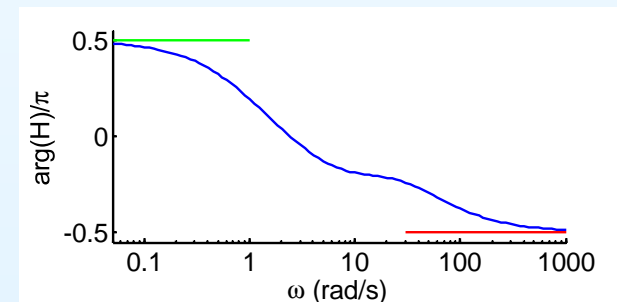
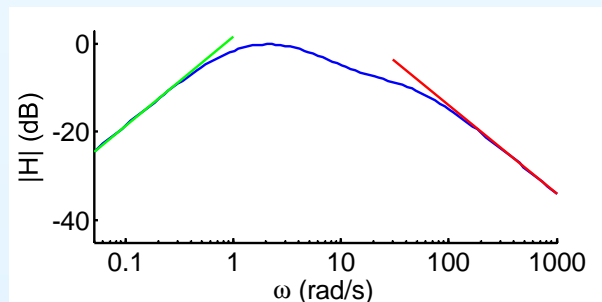
LF and HF Asymptotes

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- Frequency response is always a ratio of two polynomials in $j\omega$ with real coefficients that depend on the component values.
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$$\text{Example: } H(j\omega) = \frac{60(j\omega)^2 + 720(j\omega)}{3(j\omega)^3 + 165(j\omega)^2 + 762(j\omega) + 600}$$



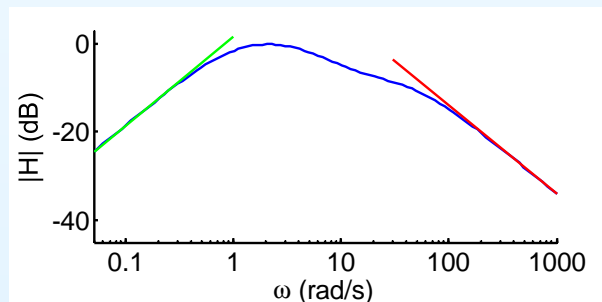
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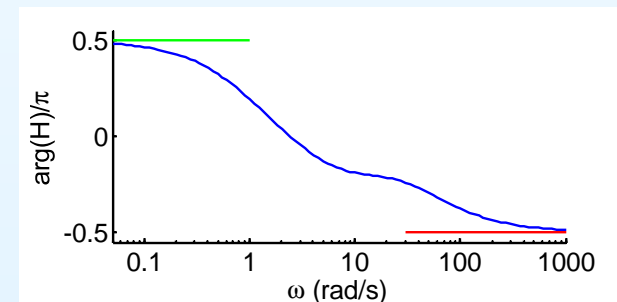
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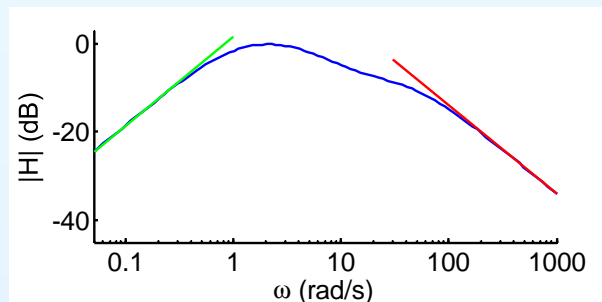
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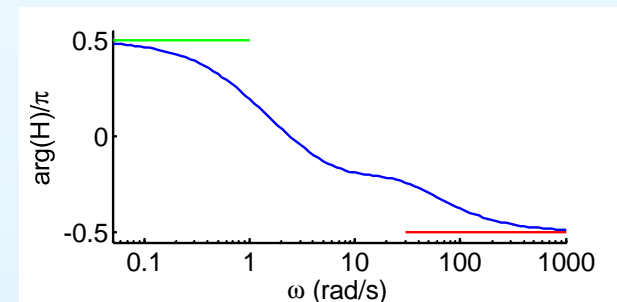
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$$\text{LF: } H(j\omega) \simeq 1.2j\omega$$

$$\text{HF: } H(j\omega) \simeq 20(j\omega)^{-1}$$



Corner frequencies (linear factors)

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- We can factorize the numerator and denominator into linear terms of the form $(aj\omega + b) \simeq \begin{cases} b & \omega < \left| \frac{b}{a} \right| \\ aj\omega & \omega > \left| \frac{b}{a} \right| \end{cases}$.

Corner frequencies (linear factors)

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- The phase changes by $\pm \frac{\pi}{2}$ because the linear term introduces another factor of j into the numerator or denominator for $\omega > \omega_c$.
 - The phase change is **gradual** and takes place over the range $0.1\omega_c$ to $10\omega_c$ ($\pm \frac{\pi}{2}$ spread over two decades in ω).

Corner frequencies (linear factors)

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- When a and b are real and positive, it is often convenient to write $(aj\omega + b) = b \left(\frac{j\omega}{\omega_c} + 1 \right)$.

Corner frequencies (linear factors)

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- When a and b are real and positive, it is often convenient to write $(aj\omega + b) = b \left(\frac{j\omega}{\omega_c} + 1 \right)$.
- The **corner frequencies** are the absolute values of the roots of the numerator and denominator polynomials (values of $j\omega$).

Sketching Magnitude Responses (linear factors)

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3. At a corner frequency, the gradient of the magnitude response changes by ± 1 (± 20 dB/decade). $+$ for numerator (top line) and $-$ for denominator (bottom line).
4. $|H(j\omega_2)| = \left(\frac{\omega_2}{\omega_1}\right)^k |H(j\omega_1)|$ if the gradient between them is k .

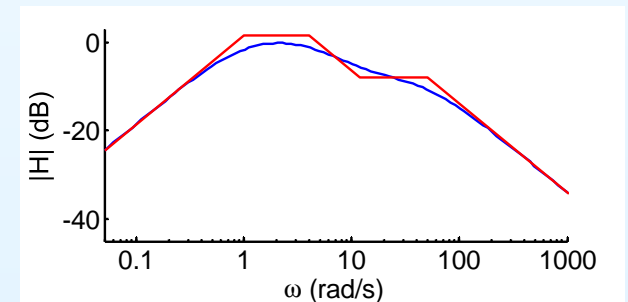
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Sketching Magnitude Responses (linear factors)

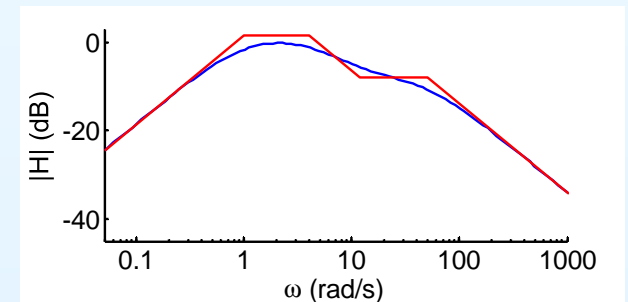
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$$\text{LF: } 1.2j\omega \Rightarrow |H(j1)| = 1.2 \text{ (1.6 dB)}$$



Sketching Magnitude Responses (linear factors)

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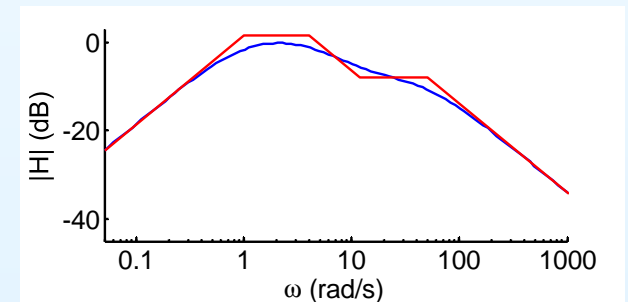
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Sketching Magnitude Responses (linear factors)

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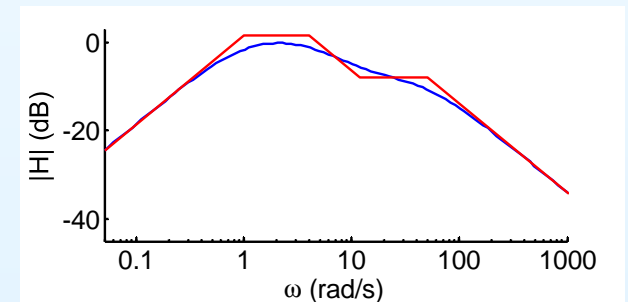
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Sketching Magnitude Responses (linear factors)

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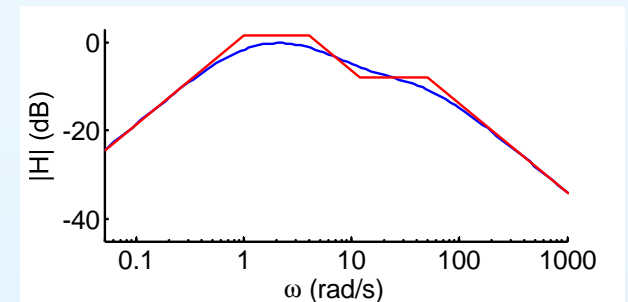
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$$|H(j50)| = \left(\frac{50}{12}\right)^0 \times 0.4 = 0.4 \text{ (-8 dB)}.$$



Sketching Magnitude Responses (linear factors)

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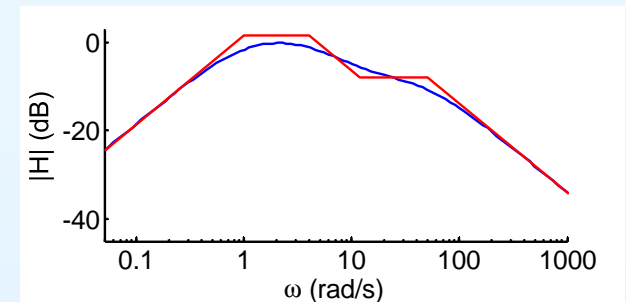
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Filters

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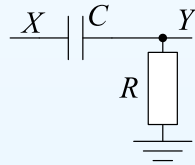
- Filter: a circuit designed to amplify some frequencies and/or attenuate others. Very widely used.
- The **order** of the filter is the highest power of $j\omega$ in the denominator of the frequency response.
- Often use op-amps to provide a low impedance output.

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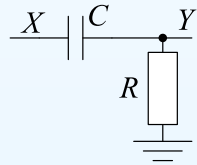
$$\frac{Y}{X} = \frac{R}{R + 1/j\omega C}$$

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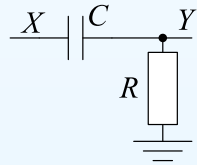
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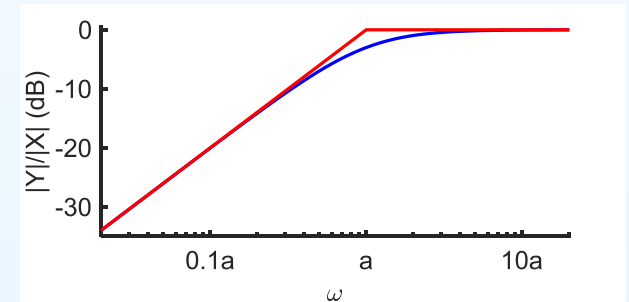
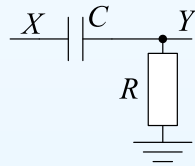
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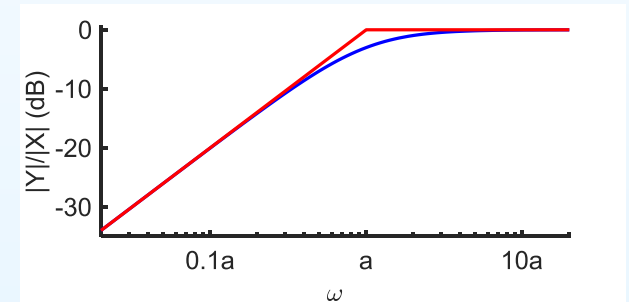
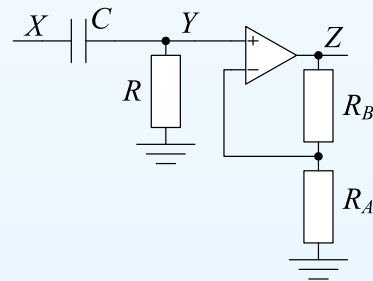
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Filters

Revision Lecture 1: Nodal Analysis & Frequency Responses

- Exam
- Nodal Analysis
- Op Amps
- Block Diagrams
- Diodes
- Reactive Components
- Phasors
- Plotting Frequency Responses
- LF and HF Asymptotes
- Corner frequencies (linear factors)
- Sketching Magnitude Responses (linear factors)
- **Filters**
- Resonance

- Filter: a circuit designed to amplify some frequencies and/or attenuate others. Very widely used.
- The **order** of the filter is the highest power of $j\omega$ in the denominator of the frequency response.
- Often use op-amps to provide a low impedance output.



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$$\frac{Z}{X} = \frac{Z}{Y} \times \frac{Y}{X} = \left(1 + \frac{R_B}{R_A}\right) \times \frac{j\omega RC}{\frac{j\omega}{a} + 1}$$

Resonance

- Resonant circuits have quadratic factors that cannot be factorized

- $H(j\omega) = a(j\omega)^2 + bj\omega + c = c \left(\left(\frac{j\omega}{\omega_0} \right)^2 + 2\zeta \left(\frac{j\omega}{\omega_0} \right) + 1 \right)$

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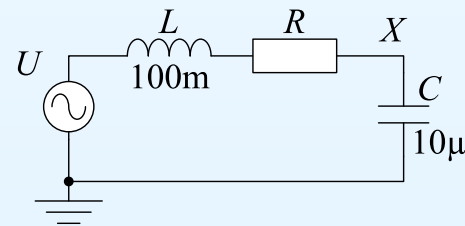
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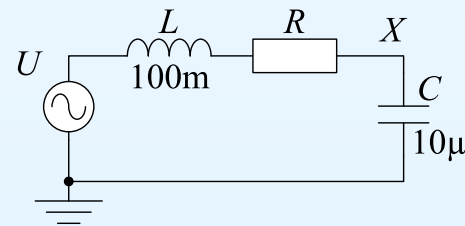
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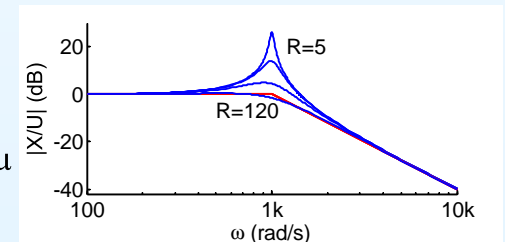
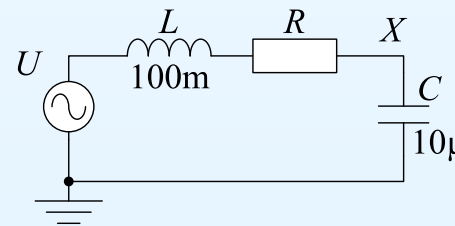
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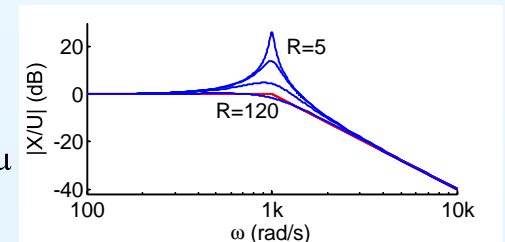
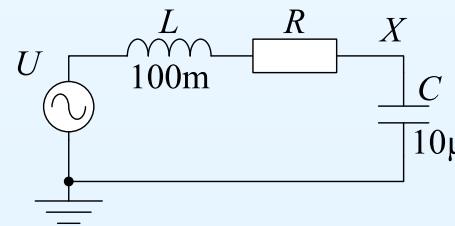
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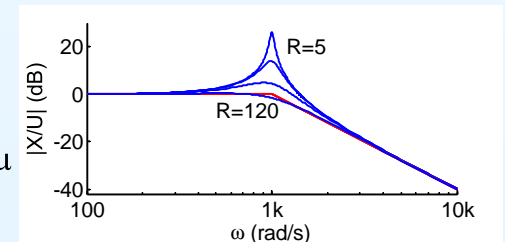
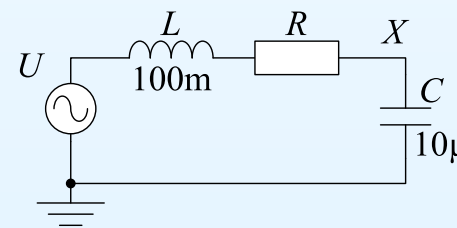
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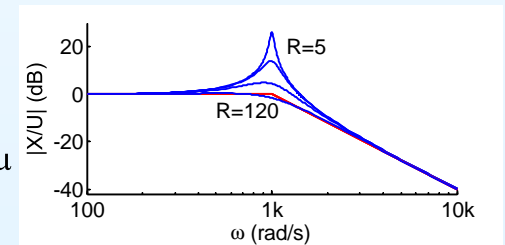
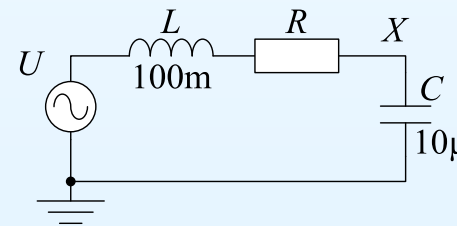
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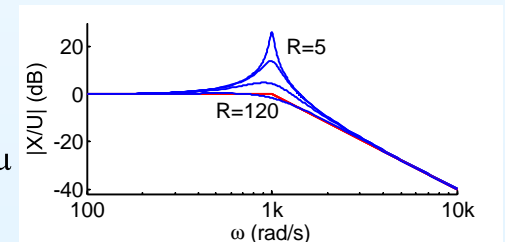
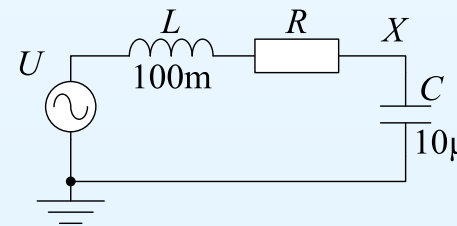
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